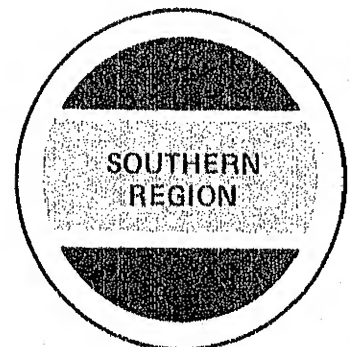


**HYMO:  
PROBLEM-ORIENTED COMPUTER LANGUAGE  
FOR HYDROLOGIC MODELING  
Users Manual**

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In Cooperation With

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# HYMO: PROBLEM-ORIENTED COMPUTER LANGUAGE FOR HYDROLOGIC MODELING

## Users Manual

By Jimmy R. Williams<sup>1</sup> and Roy W. Hann, Jr.<sup>2</sup>

### INTRODUCTION

HYMO (7)<sup>3</sup> is a problem-oriented computer language for modeling surface runoff and sediment yield from watersheds. The language is called HYMO from the words "hydrologic model." HYMO was designed for planning flood prevention projects, forecasting floods, and research studies. It consists of a main program and 16 subroutines written in FORTRAN IV, but it can be used by hydrologists with little knowledge of computer programming. The language provides 17 commands for the hydrologist to use in any sequence for application to any watershed.

HYMO was designed to transform rainfall data into runoff hydrographs and to route these hydrographs through streams and valleys or reservoirs. It will also compute the amount of sediment produced by a storm at any point on a watershed. It will be useful to research hydrologists in studying the effects of watershed and storm characteristics on the flood hydrograph. HYMO is also a good research tool for testing

hydrologic procedures; for example, a new flood-routing method could be added to HYMO and tested easily, because the inflow hydrographs and the rating curves are available in a HYMO program.

HYMO is flexible. Present hydrologic procedures can be modified or deleted, and other hydrologic procedures can be added by hydrologists familiar with FORTRAN IV programming. Adding a new command simply requires the addition of a new subroutine.

HYMO is efficient, practical, and generally applicable. HYMO programs can be written and the results interpreted by hydrologists who have no conventional computer programming experience. The hydrologic procedures used in HYMO are practical — required inputs are easy to obtain for most watersheds.

HYMO was written for the IBM 360-65 computer, but it could be run on an IBM 1130 with little modification. The storage requirement is about 73 K.

### OPERATION OF HYMO

HYMO consists of a main program and 16 subroutines. The HYMO card deck is set up in the following order:

1. Main program.
2. Subroutines.
3. A data card containing the number of commands in the command table.
4. A data card containing the ZALFA array.
5. Seventeen data cards containing the command table.
6. The users program deck consisting of program and data cards.

A printout of the main program, subroutines, ZALFA array, and command table is given in the appendix.

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<sup>3</sup>Italicized number in parentheses refer to items in "Literature Cited" preceding the appendix.

The main program reads the command table and then calls the HONDO subroutine (2) to read a program data card. Subroutine HONDO determines the command name and number by comparing columns 1 through 20 of the program data card with the command table. Then HONDO determines individual data items by comparing columns 21 through 80 of the pro-

gram data card with the ZALFA array. The data are placed in an array and returned to the main program. Based on the command number, the main program calls the proper subroutine to do the desired calculations. When the calculations are complete, control is returned to the main program, and HONDO is called again to read the next program card.

## HYDROLOGIC PROCEDURES USED IN HYMO

The procedures used in HYMO were selected because of their accuracy, general applicability, practicality of inputs, and computational efficiency. For most watersheds the input is easy to obtain, and the procedures produce reasonably accurate results without excessive computer time.

### Hydrograph Computation

When flood routing is performed, a watershed is divided into many small areas according to its hydraulic characteristics. The hydrographs from these areas must be estimated, since streamflow measurements are seldom available. A procedure for computing unit hydrographs was developed previously (4). A modification of this procedure is used in HYMO. Unit hydrographs are divided into three parts for computation (fig. 1). From the beginning of rise to the inflection point,  $t_0$ , the hydrograph is computed by the two-parameter gamma distribution equation

$$q = q_p \left[ \frac{t}{t_p} \right]^{(n-1)} e^{-(1-n)(t/t_p-1)} \quad (1)$$

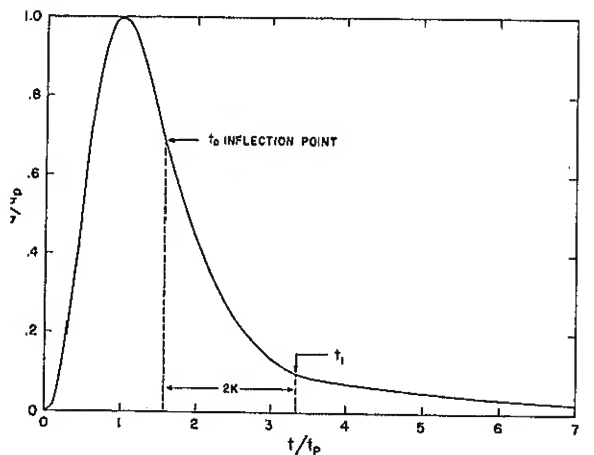


Figure 1. Dimensionless unit hydrograph.

where  $q$  = flow rate in cubic feet per second at time  $t$ ,  
 $q_p$  = peak flow rate in cubic feet per second,  
 $t_p$  = time to peak in hours,  
 and  $n$  = dimensionless parameter.

From  $t_0$  to  $t_1$  ( $t_1 = t_0 + 2K$ ) the hydrograph is computed by the recession depletion equation

$$q = q_0 e^{-\frac{t_0-t}{K}} \quad (2)$$

where  $q_0$  = flow rate at the inflection point,  
 $t_0$  = time at the inflection point,  
 and  $K$  = recession constant in hours.

From  $t_1$  to  $\infty$  the recession depletion equation becomes

$$q = q_1 e^{-\frac{t_1-t}{K_1}} \quad (3)$$

where  $q_1$  = flow rate at  $t_1$ ,  
 and  $K_1 = 3K$  = second recession constant.

The dimensionless shape parameter,  $n$ , is a function of  $K/t_p$ , as shown in figure 2. The peak flow rate is computed by the equation

$$q_p = \frac{BAQ}{t_p} \quad (4)$$

where  $B$  = a watershed parameter, a function of  $n$  as shown in figure 3,

$A$  = watershed area in square miles,  
 and  $Q$  = volume of runoff in inches.

Therefore, the entire unit hydrograph can be computed if  $K$  and  $t_p$  are known.  $K$  and  $t_p$  can be determined by hydrograph analysis (4) for gaged watersheds. To compute  $K$  and  $t_p$  for ungaged watersheds, HYMO uses the equations

$$K = 27.0A^{0.231}SLP^{-0.777}(L/W)^{0.124} \quad (5)$$

$$\text{and } tp = 4.6340.422SLP - 0.46(L/W)0.133 \quad (6)$$

where  $SLP$  = difference in elevation in feet, divided by flood-plain distance in miles, between watershed outlet and most distant point on the watershed,  
and  $L/W$  = watershed length-width ratio.

Storm hydrographs are computed by convolving unit hydrographs with incremental source runoff. To compute incremental source runoff, the mass rainfall curve is broken into equal time increments, and the Soil Conservation Service (SCS) rainfall-runoff relationship (3) is applied. The SCS rainfall-runoff relationship is expressed in a set of numbered curves. The SCS National Engineering Handbook (3) provides detailed instructions for selecting the proper curve number.

Hydrographs computed by this procedure compared closely with measured hydrographs from 34 watersheds located in Texas, Oklahoma, Arkansas, Louisiana, Mississippi, and Tennessee. The watershed areas ranged from 0.5 to 25 square miles.

### Flood Routing

#### Streams and valleys

The variable storage coefficient (VSC) flood-routing method (5) was selected for HYMO.

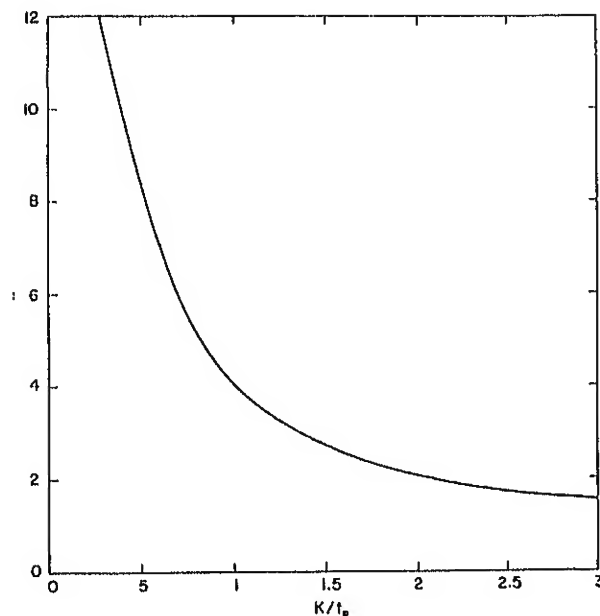


Figure 2. Relationship between dimensionless shape parameter and recession constant/time to peak.

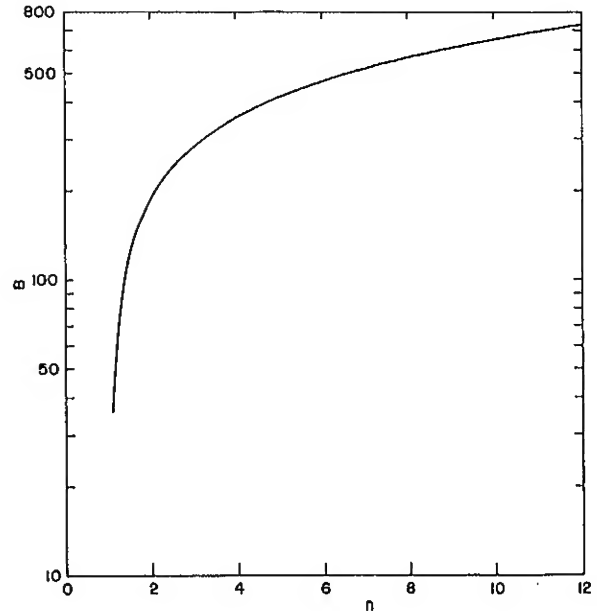


Figure 3. Relationship between dimensionless shape parameter  $n$  and watershed parameter  $B$ .

The VSC method has been revised (6) to account for the variation in water surface slope during a flood. The revised VSC method is about as accurate as the implicit method (1) and has the general applicability of simpler storage methods. Although an iterative solution is used, the VSC method requires little computer time and is free of convergence problems.

The VSC routing equations are

$$O_2 = C_2 \left[ I_2 + \left( \frac{1}{C_1} - 1 \right) O_1 \right] \quad (7)$$

$$C_2 = \frac{2 \Delta t}{2T_2 + \Delta t} \quad (8)$$

$$C_1 = \frac{2 \Delta t}{2T_1 + \Delta t} \quad (9)$$

$$T_1 = \left( \frac{L}{1800(V_{I_1} + V_{O_1})} \right) \times \left( \frac{L \times SLP_0}{L \times SLP_0 + D_{I_1} - D_{O_1}} \right)^{1/2} \quad (10)$$

$$T_2 = \left( \frac{L}{1800(V_{I_2} + V_{O_2})} \right) \times \left( \frac{L \times SLP_0}{L \times SLP_0 + D_{I_2} - D_{O_2}} \right)^{1/2} \quad (11)$$



In these equations subscripts 1 and 2 refer to the beginning and end of the time interval  $\Delta t$ ; the units are cubic feet per second for flow, hours for time, feet per second for velocity, and feet for length and depth. The symbols are defined as follows:

$I$  = inflow rate.  
 $O$  = outflow rate.  
 $I_a = \frac{I_1 + I_2}{2}$  = average inflow rate.  
 $C$  = storage coefficient.  
 $T$  = travel time through the reach.  
 $L$  = reach length.  
 $V$  = velocity.  
 $SLP_0$  = normal slope.  
 $D$  = depth.

Since  $T_2$  and  $C_2$  are dependent upon  $O_2$ , an iterative technique is required to solve the routing equations. In equation 7,  $I_a$  and  $O_1$  are known, and  $C_1$  can be computed from equation 9. This leaves only  $O_2$  and  $C_2$  as unknowns.  $O_1$  can be used as a first approximation of  $O_2$ . The normal depth and velocity for the approximate value of  $O_2$  are entered into equation 11 for computing  $T_2$ . Then equation 8 is used to compute  $C_2$ . The second approximation of  $O_2$  is then obtained from equation 7. This iterative process continues until the difference between successive  $O_2$  values is acceptable. HYMO is set to accept differences of 0.1 percent or less. Usually about four iterations are required.

#### Reservoirs

HYMO uses the storage-indication method (3) to route floods through reservoirs. This method has been widely used and accepted because it is practical and accurate. The SCS National Engineering Handbook gives detailed instructions for using the method.

## RULES FOR USING HYMO

The reader should refer to the table, "Example Input for HYMO Commands," as he follows the narrative description of the rules. The example HYMO program that is presented near the end of the manual may also be helpful.

#### General Rules

HYMO commands are expressed in the first 20 columns of the data card, and columns 21

#### Rating Curves

Rating curves must be available at enough locations along a valley to adequately describe the hydraulics of the stream and valley. Most of these rating curves must be computed because there are never enough measured rating curves.

HYMO uses Manning's equation to compute the normal flow-rating curves that are used in the VSC flood-routing method. The normal flood-plain slope is determined for each valley section by plotting a profile of the flood plain. The normal channel slope is determined by plotting a profile of the flood plain with channel distances.

#### Sediment Yields

The universal soil loss equation (8) was modified to compute the sediment yield for individual storms on watersheds. The modified equation is

$$S = 95 (q_p \times Q)^{0.56} \times K \times C \times P \times LS, \quad (12)$$

where  $S$  = sediment yield in tons,  
 $q_p$  = peak flow rate in cubic feet per second,  
 $Q$  = volume of runoff in acre-feet,  
 $K$  = the soil-erodibility factor,  
 $C$  = the cropping-management factor,  
 $P$  = the erosion control practice factor,  
and  $LS$  = the slope length and gradient factor.

Detailed instructions for determining  $K$ ,  $C$ ,  $P$ , and  $LS$  are given by Wischmeier and Smith (8).

Since equation 12 was designed to compute sediment yield from watersheds, a delivery ratio is not needed. The delivery ratio is built into equation 12 by including the peak flow rate. Many of the watershed characteristics that influence the peak flow rate also affect the delivery ratio. Equation 12 has performed well under limited testing, but future refinements are expected.

through 79 are used for numeric data and keywords. Column 80 is reserved for a page-change code (an asterisk in column 80 causes the card to be printed on a new page). Continuation cards are allowed when 59 characters are insufficient to express the data.

The data can be written in any format, but at least one blank space must be left between data items. A decimal is required for numbers con-

taining fractions, but not for whole numbers. Keywords can be written with the data to describe individual data items. Comment cards may be used at any point in a HYMO program by punching an asterisk in column 1 and the comment in columns 2 through 79.

*Example input for HYMO commands*

| Command              | Required input  |
|----------------------|---|
| START                | RAINFALL BEGINS AT 12.5 HRS      PUNCH CODE=1   |
| STORE HYD            | ID=1    HYD NO=301    DT=.2 HR    DA=1.5 SQ MI<br>FLOW RATES= 0 10 50 100 500 1000 1800 2000 1900 1500 1200<br>1000 800 600 500 400 300 200 100 50 10 1   |
| COMPUTE HYD          | ID=2    HYD NO=302    DT=.5 HR    DA=2.1 SQ MI    CN=90<br>HT=100 FT    L=3.3 MI<br>MASS RAINFALL = 0 .31 .61 1.04 1.84 2.74 3.06 3.45 4.33 4.75  |
| PRINT HYD            | ID=2    CODE=1  |
| PUNCH HYD            | ID=2  |
| PLOT HYD             | ID I=3    ID II=4   |
| ADD HYD              | ID=4    HYD NO=101    ID I=5    ID II=6   |
| STORE RATING CURVE   | ID=2    VS NO=15<br>ELEV      AREA      FLOW<br>496.6      0          0<br>497        2          1<br>498        9          19<br>499        19        52<br>500        30        98  |
| COMPUTE RATING CURVE | ID=1 VS NO=10 NO SEGS=3 MIN ELEV=482 FT MAX ELEV=492 FT<br>CH SLP=.006    FP SLP=.0075    N=.05 DIST=175 FT<br>N=-.03    DIST=205 FT    N=.05 DIST=450 FT<br>DIST    ELEV    DIST    ELEV    DIST    ELEV    DIST    ELEV<br>0    492.0    100    490.0    175    484.0    188    482.0<br>190    482.0    205    484.0    250    486.0    275    488.0<br>310    490.0    450    492.0 |
| COMPUTE TRAVEL TIME  | ID=3    REACH NO=8    NO VS=5    L=4500 FT    SLP=.0075   |
| ROUTE                | ID=3    HYD NO=8    INFLOW ID=6    DT=.25 HR  |
| ROUTE RESERVOIR      | ID=5    HYD NO=501    INFLOW ID=1<br>OUTFLOW (CFS)      STORAGE (AC FT)<br>0                    0<br>22                   533<br>200                   555<br>1000                  601<br>2000                  648<br>3000                  694   |
| ERROR ANALYSIS       | ID I=3    ID II=5   |
| SEDIMENT YIELD       | ID=5    SOIL=.34    CROP=.5    EP=.6    LS=.3   |
| FINISH               |   |

Six hydrographs can be stored in a HYMO program at a time. The hydrographs are identified by storage location numbers 1 through 6. Therefore, the same storage location number must be used for many hydrographs in a HYMO program. This is especially true when routing is done through large watersheds. However, no more than six hydrographs are ever needed at one time because HYMO programs begin at the head of a watershed and work downstream through one reach at a time. When a storage location number is used to store or compute another hydrograph, the first hydrograph is lost. The user should be sure that the hydrograph will not be referred to again before using the storage location number for another command.

To store, compute, or route a hydrograph, the user must specify the time increment. There are no rigid rules about selecting the time increment, but generally it should not be greater than one-fifth of the time to the peak of the hydrograph. This rule usually provides enough points to adequately define the hydrograph. All hydrographs are limited to 300 points.

For the commands "STORE HYD," "COMPUTE HYD," "ADD HYD," "ROUTE," and "ROUTE RESERVOIR," the user must specify the number of the outflow hydrograph. The hydrograph identification numbers are used to designate specific routing reaches, incremental areas, reservoirs, and partial hydrographs. The partial hydrograph number is given to all hydrographs other than outflow hydrographs from reaches, incremental areas, or reservoirs. The identification numbers for each group are

|                               |         |
|-------------------------------|---------|
| Reaches . . . . .             | 1-100   |
| Partial hydrographs . . . . . | 101-300 |
| Incremental areas . . . . .   | 301-500 |
| Reservoirs . . . . .          | 501+    |

### Command Rules

The first command for any watershed is START. The two data items associated with this command are the time rainfall begins on the watershed and a code for punching output data. If a storm is to be routed through a watershed only once, the punch code is deleted. However, if more than one routing is to be performed, set the punch code equal to a positive number, and the output data for the first routing will be

punched for use in the second routing. More than one routing is usually required.

Two commands, RECALL HYD and STORE TRAVEL TIME, were designed to be computer punched for second routings; consequently, these commands do not appear in the table.

The STORE HYD command is used to store the coordinates of a hydrograph in the computer. It can be used for storing measured hydrographs or hydrographs computed by methods other than the one used in HYMO. The input data required for STORE HYD are storage location number, hydrograph identification number, time increment, watershed area, and flow rates of the hydrograph at the specified time increment.

The COMPUTE HYD command is used to compute hydrographs from the incremental areas of the watershed. The first five items of data are storage location number, hydrograph identification number, time increment, watershed area, and SCS runoff curve number (3). Normally, data items 6 and 7 are watershed height and main stem length. The height and length are used to compute the recession constant  $K$  and the time to peak  $t_p$ . However, if  $K$  and  $t_p$  are known or estimated by some other method, they can be entered directly into the program. This is accomplished by placing a minus sign before the values of  $K$  and  $t_p$  and entering them as data items 6 and 7, respectively. The remaining data items are values of the mass rainfall at the specified time increment.

Since most watersheds have a limited number of rain gages, the same mass rainfall data may be used to develop several hydrographs. Once the mass rainfall data have been entered in a COMPUTE HYD command, they can be repeated for any number of COMPUTE HYD commands without repunching the data. Instead, punch a negative number for the eighth data item of all COMPUTE HYD commands that use the same rain gage. When data from another rain gage are entered, the data from the first rain gage are lost and cannot be recalled by using the negative number code.

The RECALL HYD command is one of the two commands that are computer punched. When the punch code is a positive number, the output from STORE HYD and COMPUTE HYD are punched on cards with the RECALL HYD command. The RECALL HYD command stores

the computed and stored hydrographs on cards; it is therefore not necessary to recompute hydrographs for future routings. Instead, the previously computed hydrographs are read into the program, thus saving considerable computer time.

Although the input data for the RECALL HYD command are never punched manually, a list of the data items may be helpful in checking computer-punched cards. The input data are storage location number, hydrograph identification number, time increment, drainage area, peak flow rate, runoff volume, number of hydrograph points, and flow rates of the hydrograph.

The PRINT HYD command is used to print coordinates of a hydrograph, volume of runoff, and peak flow rate. The required input data are the storage location number and a peak-volume code. The peak-volume code is deleted if a complete hydrograph printout is desired. If a printout of only the runoff volume and the peak flow rate is needed, the peak-volume code is set to a positive value.

The PUNCH HYD command is used to punch any hydrograph in a HYMO program in the proper form for the RECALL HYD command. PUNCH HYD has two purposes: (1) If the punch code is not used, PUNCH HYD can be used to punch one or more hydrographs for future use; and (2) if it is desirable to punch outflow hydrographs associated with ROUTE, ROUTE RESERVOIR, or ADD HYD, PUNCH HYD must be used because the punch code only provides for punching hydrographs associated with STORE HYD and COMPUTE HYD. The only datum required for PUNCH HYD is the storage location number of the hydrograph to be punched.

The PLOT HYD command is used to plot hydrographs in a HYMO program. It will plot one hydrograph on a set of axes, or if a comparison is desired, it will plot two hydrographs on the same set of axes. The required input data are the storage location numbers of the hydrographs to be plotted.

The ADD HYD command adds the coordinates of any two hydrographs. The hydrographs are added at a time increment equal to that of the hydrograph with the shorter time increment. The only data required are the storage location number and hydrograph identification number

of the added hydrograph and the storage location numbers of the two hydrographs to be added.

The STORE RATING CURVE command is used to store rating curves that have been measured or computed previously. STORE RATING CURVE will save considerable computer time if measured or computed rating curves are available. The input data are the storage location number, valley section number, and individual rating curve points described by elevation, end-area, and flow rate. The number of points used to describe a rating curve is limited to 20.

The COMPUTE RATING CURVE command is used to compute the stage-area-flow relationship for a valley section. The input data are storage location number, valley section number, number of segments in the valley section, minimum elevation, maximum elevation, channel and flood-plain slopes, Manning's  $n$  value and segment boundary point for each segment, and horizontal and vertical position of points describing the valley section.

The storage location numbers of the valley sections in a particular reach must begin with 1 and increase by one for each valley section in the reach. However, the numbers are assigned without regard to upstream or downstream order. The valley section identification number can be any number from 0.1 to 999.9. These rules concerning storage location and valley section identification numbers also apply to the STORE RATING CURVE command.

Normally, valley sections are divided into three segments (two flood-plain segments and a channel segment) for computing the rating curve. However, some valley sections may have more than one channel or may have an extreme variation in  $n$  values across the flood plain, thus requiring more than three segments. A maximum of six segments is permitted. Manning's  $n$  values for each segment are input with segment boundary point (distance from the beginning of the valley section to the end of the segment). Flood-plain  $n$  values are positive and channel  $n$  values are negative.

Twenty points are used to define a rating curve. The location of the points is determined by dividing the difference between the maximum and minimum elevations into 19 equal increments.

The COMPUTE TRAVEL TIME command is used to compute the normal flow travel time relationship used in ROUTE. The input data are storage location number, reach identification number, number of valley sections in the reach, reach length, and slope. The reach identification number can be any number from 0.1 to 999.9. The maximum number of valley sections per reach is six. The slope can be either the channel or flood-plain slope or a weighted average of the two. If flow is confined to the channel, the channel slope is of course applicable. If most of the flow is in the flood plain, usually the flood-plain slope is used. However, a weighted slope based on the relative rates of flow in the channel and the flood plain may be used.

The COMPUTE TRAVEL TIME command considers each rating curve in the reach in computing the travel time flow relationship. COMPUTE TRAVEL TIME automatically selects the flow rates that are used in computing individual travel times. The flow rates of the rating curve with the lowest maximum flow rate are chosen. If the flow rates of any other rating curve in the reach were chosen, the rating curve with the lowest maximum flow rate would have to be extrapolated. The travel time table is limited to 19 points because of the 20-point limit for rating curves.

The STORE TRAVEL TIME command is one of the two computer-punched commands. When the punch code is a positive number, the output from COMPUTE TRAVEL TIME is punched on cards with the STORE TRAVEL TIME command. Therefore, it is not necessary to recompute rating curves or travel time for future routings. Instead, STORE TRAVEL TIME reads the previously computed travel time flow relationship into the program, thus saving considerable computer time.

The input data for STORE TRAVEL TIME are not punched manually, but a list of data items may be helpful in checking computer-punched cards. The input data are storage location number, reach identification number,

reach length, slope, and individual points of the relationship defined by depth, flow, and travel time.

The ROUTE command is used to route floods through streams and valleys. The input data are storage location number and hydrograph identification number of the outflow hydrograph, storage location number of the inflow hydrograph, and time increment. The storage location number of the outflow hydrograph must be the same as the storage location number used in COMPUTE TRAVEL TIME for the reach. To prevent unnecessary program stoppage, ROUTE extrapolates the travel-time table when it is exceeded and writes the message, "TRAVEL TIME TABLE EXCEEDED."

The ROUTE RESERVOIR command is used to route floods through reservoirs. The input data are storage location number and hydrograph identification number of the outflow hydrograph, storage location number of the inflow hydrograph, and individual points of the reservoir's outflow-storage relationship. The outflow-storage relationship must be expressed in 20 points or less. If the outflow-storage relationship is exceeded, ROUTE RESERVOIR will extrapolate the relationship and write the message, "STORAGE-DISCHARGE TABLE EXCEEDED."

The ERROR ANALYSIS command is used to determine the error standard deviation and the percentage error in peak flow between any two hydrographs in a HYMO program. These functions make ERROR ANALYSIS useful in research. The input data are the storage location numbers of the two hydrographs to be analyzed.

The SEDIMENT YIELD command is used to compute the sediment yield at any point in a watershed. Input data required are storage location number of the hydrograph from the area, a soils factor, a crop factor, a slope length and gradient factor, and a conservation practice factor (8).

The FINISH command is used to end HYMO programs. There are no data associated with FINISH.

## EXAMPLE HYMO PROGRAM

A short example problem is presented to demonstrate HYMO. Figure 4 is a map of the 6.84-square-mile Brushy Creek watershed near

Riesel, Tex. A flood will be routed through the watershed in its present condition, and the routed outflow hydrograph will be compared to

the hydrograph measured at gaging station G. Also the sediment yield will be predicted and compared with the measured sediment yield. Then the same flood will be routed through the watershed with two proposed reservoirs. To determine the effects of the reservoirs, the outflow hydrograph and sediment yield will be compared to the outflow hydrograph and sediment yield of the present-condition routing.

Comment cards and keywords are used liberally in the example problem to acquaint the user with HYMO. After becoming familiar with HYMO, the user may write fewer comments and keywords, but generally users find them both quite helpful in describing the problem. To save space in the example problem, few of the hydrographs are printed or plotted. Some users may choose to print and plot all hydrographs.

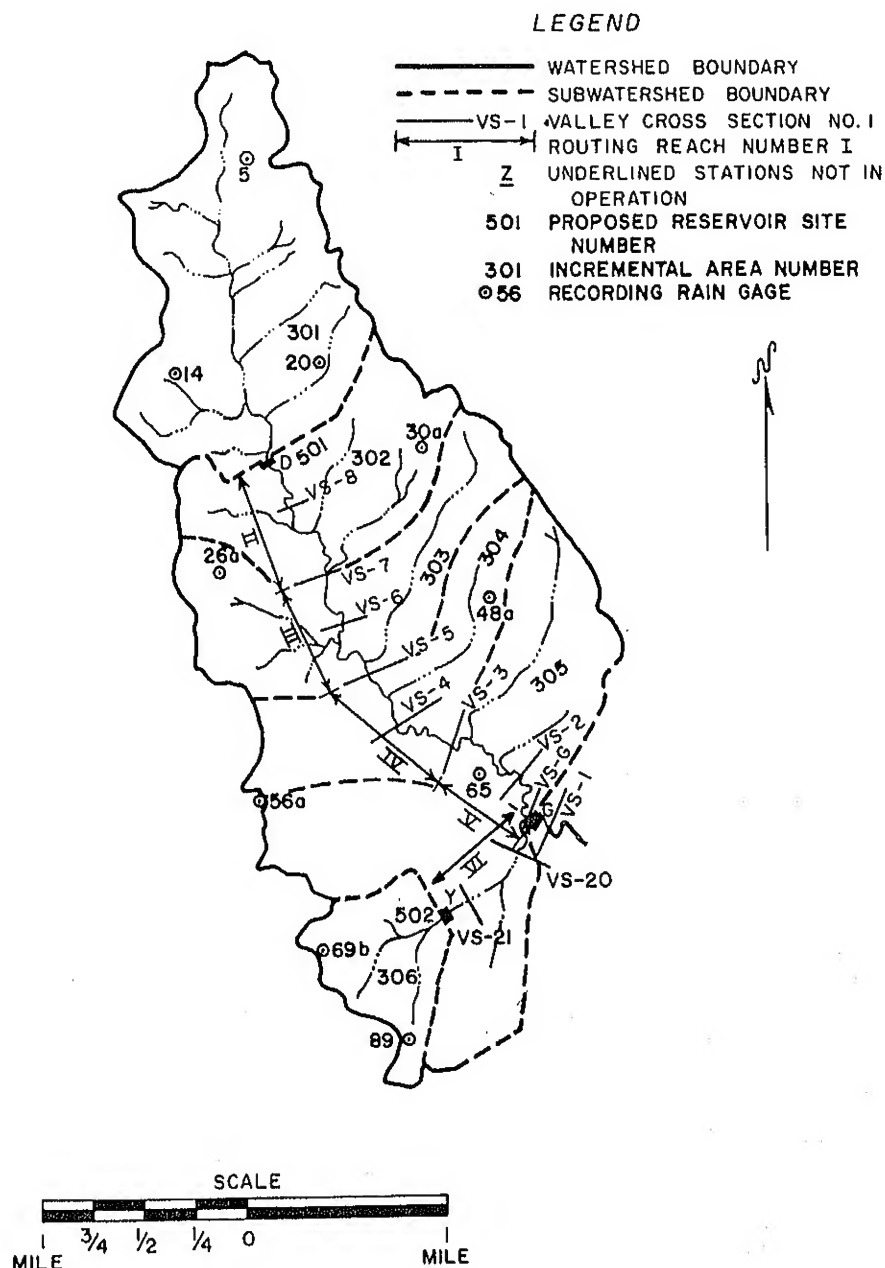


Figure 4. Brushy Creek watershed near Riesel, Tex.

## EXAMPLE HYMO PROGRAM

```

* * TO PRINT ON A NEW PAGE AN ASTERISK IS PUNCHED IN COLUMN 80.
* * COMMENTS ARE WRITTEN AT ANY POINT IN A HYMO PROGRAM BY PUNCHING AN
* * ASTERISK IN COLUMN 1 AND THE COMMENT IN COLUMNS 2 - 79.
* * THE FLOOD OF MARCH 29, 1965 WILL BE ROUTED THROUGH THE BRUSHY CREEK WATERSHED
* * NEAR RIESEL, TEXAS.
* * TIME RAINFALL BEGINS ON THE WATERSHED, AND TO INDICATE THE PUNCH CODE. THE
* * PUNCH CODE IS USED TO PUNCH THE OUTPUT FOR USE IN FUTURE ROUTINGS. IF ONLY
* * ONE ROUTING IS PLANNED, THE PUNCH CODE IS DELETED.
* *
START      RAINFALL BEGINS AT 12.5 HRS   PUNCH CODE=1
*
* BEGINNING AT THE TOP OF THE WATERSHED THE FIRST STEP IS TO DETERMINE THE
* * HYDROGRAPH FROM AREA 301. IT IS NOT NECESSARY TO COMPUTE THE HYDROGRAPH,
* * BECAUSE IT WAS MEASURED PREVIOUSLY. THE STORE HYD COMMAND IS USED TO STORE
* * THE MEASURED HYDROGRAPH IN THE PROGRAM.
* *
STORE HYD      ID=1   HYD NO=301   DT=.1666667 HRS   DA=1.734 SQ MI
REMAINING DATA ARE FLOW RATES BEGINNING AT
START TIME AND INCREMENTED BY DT 0 0 0 0 0
20 90 220 1025 1420 1380 2085 2260 2360 2110 1885 1890 1760
1560 1350 1150 1000 860 690 560 460 370 365 380 400 415
395 370 330 300 270 235 200 175 160 140 130 120 110 110
110 110 100 100 90 80 70 65 60 50 47 44 41 38 35 33 31 29
27 25 23 22 20 18 17 16 15 14 13 12 11 10 10 9 8 8 7 7 6
6 6 5 5 4 4 4 4 3 3 3 3 2 2 1
* THE PRINT HYD COMMAND IS USED TO PRINT THE HYDROGRAPH FROM AREA 301.
PRINT HYD      ID=1

```

## HYDROGRAPH FROM AREA 301

| TIME<br>HRS | FLOW<br>CFS | TIME<br>HRS | FLOW<br>CFS | TIME<br>HRS | FLOW<br>CFS | TIME<br>HRS | FLOW<br>CFS | TIME<br>HRS | FLOW<br>CFS |
|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| 12.500      | 0.          | 16.000      | 1150.       | 19.500      | 140.        | 23.000      | 33.         | 26.499      | 8.          |
| 12.667      | 0.          | 16.167      | 1000.       | 19.666      | 130.        | 23.166      | 31.         | 26.666      | 7.          |
| 12.833      | 0.          | 16.333      | 860.        | 19.833      | 120.        | 23.333      | 29.         | 26.833      | 7.          |
| 13.000      | 0.          | 16.500      | 690.        | 20.000      | 110.        | 23.500      | 27.         | 26.999      | 6.          |
| 13.167      | 0.          | 16.667      | 560.        | 20.166      | 110.        | 23.666      | 25.         | 27.166      | 6.          |
| 13.333      | 0.          | 16.833      | 460.        | 20.333      | 110.        | 23.833      | 23.         | 27.333      | 6.          |
| 13.500      | 20.         | 17.000      | 370.        | 20.500      | 110.        | 23.999      | 22.         | 27.499      | 5.          |
| 13.667      | 90.         | 17.167      | 300.        | 20.666      | 110.        | 24.166      | 20.         | 27.666      | 5.          |
| 13.833      | 220.        | 17.333      | 365.        | 20.833      | 100.        | 24.333      | 18.         | 27.833      | 4.          |
| 14.000      | 1025.       | 17.500      | 380.        | 21.000      | 100.        | 24.499      | 17.         | 27.999      | 4.          |
| 14.167      | 1420.       | 17.667      | 490.        | 21.166      | 90.         | 24.666      | 16.         | 28.166      | 4.          |
| 14.333      | 1380.       | 17.833      | 415.        | 21.333      | 80.         | 24.833      | 15.         | 28.333      | 4.          |
| 14.500      | 2085.       | 18.000      | 395.        | 21.500      | 70.         | 24.999      | 14.         | 28.499      | 3.          |
| 14.667      | 2260.       | 18.167      | 370.        | 21.666      | 65.         | 25.166      | 13.         | 28.666      | 3.          |
| 14.833      | 2360.       | 18.333      | 330.        | 21.833      | 60.         | 25.333      | 12.         | 28.833      | 3.          |
| 15.000      | 2110.       | 18.500      | 300.        | 22.000      | 50.         | 25.499      | 11.         | 28.999      | 3.          |
| 15.167      | 1885.       | 18.666      | 270.        | 22.166      | 47.         | 25.666      | 10.         | 29.166      | 3.          |
| 15.333      | 1890.       | 18.833      | 235.        | 22.333      | 44.         | 25.833      | 10.         | 29.333      | 2.          |
| 15.500      | 1760.       | 19.000      | 200.        | 22.500      | 41.         | 25.999      | 9.          | 29.499      | 2.          |
| 15.667      | 1560.       | 19.166      | 175.        | 22.666      | 38.         | 26.166      | 9.          | 29.666      | 2.          |
| 15.833      | 1350.       | 19.333      | 160.        | 22.833      | 35.         | 26.333      | 8.          | 29.832      | 1.          |

RUNOFF VOLUME = 4.933 INCHES  
PEAK DISCHARGE RATE = 2360.0 CFS

\* THE HYDROGRAPH FROM AREA 301 IS ROUTED THROUGH REACH 2. THE FIRST STEP IS TO \*  
 \* COMPUTE RATING CURVES FOR VALLEY SECTIONS 7 AND 8.

COMPUTE RATING CURVE ID=1 VS 8 3 SEGMENTS MIN ELEV = 513.8 FT  
 MAX ELEV = 521 FT CH SLOPE = .0026 FP SLOPE = .0033

FIRST SEG .05 414  
 SECOND SEG -.03 423  
 THIRD SEG .05 602

THE REMAINING DATA DEFINE THE VALLEY CROSS SECTION

| DISTANCE | ELEV  |
|----------|-------|
| 10       | 521   |
| 18       | 518.2 |
| 30       | 519.1 |
| 150      | 518.5 |
| 200      | 518.1 |
| 325      | 517.9 |
| 345      | 516.1 |
| 357      | 516.0 |
| 370      | 517.1 |
| 390      | 516.8 |
| 414      | 514.7 |
| 416      | 513.8 |
| 419      | 513.8 |
| 423      | 515.3 |
| 450      | 514.7 |
| 464      | 516.9 |
| 474      | 516.8 |
| 483      | 514.8 |
| 492      | 516.4 |
| 550      | 518.1 |
| 600      | 520.8 |
| 602      | 521.3 |

# RATING CURVE VALLEY SECTION 8.0

| WATER SURFACE ELEV | AREA SQ FT | FLOW RATE CFS |
|--------------------|------------|---------------|
| 513.80             | 0.0        | 0.0           |
| 514.18             | 1.5        | 1.7           |
| 514.56             | 3.7        | 6.3           |
| 514.94             | 8.4        | 15.5          |
| 515.32             | 23.0       | 37.8          |
| 515.69             | 44.7       | 85.8          |
| 516.07             | 70.9       | 153.2         |
| 516.45             | 107.1      | 252.0         |
| 516.83             | 153.3      | 370.7         |
| 517.21             | 217.8      | 545.3         |
| 517.59             | 291.9      | 810.0         |
| 517.97             | 373.9      | 1064.2        |
| 518.35             | 505.3      | 1430.5        |
| 518.73             | 665.6      | 1979.6        |
| 519.10             | 858.7      | 2671.5        |
| 519.48             | 1069.9     | 3670.5        |
| 519.86             | 1284.1     | 4853.4        |
| 520.24             | 1501.3     | 6225.1        |
| 520.62             | 1721.7     | 7793.4        |
| 521.00             | 1944.8     | 9613.0        |



COMPUTE RATING CURVE ID=2 VS 7 3 SEGMENTS MIN ELEV=506.9 FT  
 MAX ELEV=515 FT CH SLOPE=.0018 PP SLOPE=.00245  
 N=.05 DIST=636 N=-.03 DIST=657 N=.05 DIST=2000  
 DIST ELEV DIST ELEV DIST ELEV DIST ELEV  
 0 515.0 100 514.0 600 510.6 636 511.3  
 390 513.6 550 512.0 657 510.8 748 510.4  
 641 506.9 647 506.9 850 511.7 1050 512.7  
 772 512.5 800 511.7 1800 514 2000 515  
 1200 513.1 1255 513.6

| RATING CURVE VALLEY SECTION 7.0 |                |                     |  |
|---------------------------------|----------------|---------------------|--|
| WATER<br>SURFACE<br>ELEV.       | AREA<br>SQ. FT | FLOW<br>RATE<br>CFS |  |
| 506.90                          | 0.0            | 0.0                 |  |
| 507.33                          | 2.9            | 3.2                 |  |
| 507.75                          | 6.5            | 11.0                |  |
| 508.18                          | 10.7           | 23.3                |  |
| 508.60                          | 15.6           | 40.5                |  |
| 509.03                          | 21.2           | 63.3                |  |
| 509.46                          | 27.4           | 92.1                |  |
| 509.88                          | 34.4           | 127.9               |  |
| 510.31                          | 42.0           | 171.2               |  |
| 510.74                          | 64.6           | 229.2               |  |
| 511.16                          | 127.4          | 357.5               |  |
| 511.59                          | 206.5          | 570.7               |  |
| 512.02                          | 322.2          | 806.6               |  |
| 512.44                          | 499.4          | 1204.4              |  |
| 512.87                          | 739.0          | 1780.5              |  |
| 513.29                          | 1054.1         | 2632.7              |  |
| 513.72                          | 1428.1         | 3458.4              |  |
| 514.15                          | 2074.3         | 4671.2              |  |
| 514.57                          | 2845.0         | 7184.3              |  |
| 515.00                          | 3670.1         | 10314.2             |  |

\* BEFORE ROUTING THE TRAVEL TIME - DEPTH - FLOW RELATIONSHIP MUST BE COMPUTED \*

\* FOR THE REACH.

\* COMPUTE TRAVEL TIME ID=2 REACH 2 2 VALLEY SECTIONS  
REACH LENGTH=3400 FT SLOPE=.0029

TRAVEL TIME TABLE  
REACH 2.0

| WATER<br>DEPTH<br>FEET | FLOW<br>RATE<br>CFS | TRAVEL<br>TIME<br>HRS |
|------------------------|---------------------|-----------------------|
| 0.30                   | 2.                  | 0.8317                |
| 0.68                   | 6.                  | 0.5966                |
| 1.07                   | 16.                 | 0.4981                |
| 1.58                   | 38.                 | 0.4721                |
| 2.18                   | 86.                 | 0.3899                |
| 2.75                   | 153.                | 0.3381                |
| 3.28                   | 252.                | 0.3426                |
| 3.66                   | 371.                | 0.3637                |
| 4.02                   | 545.                | 0.3593                |
| 4.45                   | 810.                | 0.3589                |
| 4.78                   | 1064.               | 0.3598                |
| 5.13                   | 1431.               | 0.3627                |
| 5.50                   | 1980.               | 0.3526                |
| 5.86                   | 2672.               | 0.3412                |
| 6.29                   | 3670.               | 0.3359                |
| 6.67                   | 4853.               | 0.3322                |
| 6.98                   | 6225.               | 0.3074                |
| 7.29                   | 7793.               | 0.2864                |
| 7.60                   | 9613.               | 0.2667                |

\* THE ROUTE COMMAND IS USED TO ROUTE THE HYDROGRAPH FROM AREA 301 THROUGH REACH\*  
 \* 2.\*

ROUTE ID=2 HYD NO=101 INFLOW HYD ID=1 TIME INTERVAL=.2 HR  
 PRINT HYD ID=2

| PARTIAL HYDROGRAPH 101 |             |             |             |             |             |             |             |             |             |
|------------------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| TIME<br>HRS            | FLOW<br>CFS | TIME<br>HRS | FLOW<br>CFS | TIME<br>HRS | FLOW<br>CFS | TIME<br>HRS | FLOW<br>CFS | TIME<br>HRS | FLOW<br>CFS |
| 12.500                 | 0.          | 16.500      | 1031.       | 20.500      | 115.        | 24.500      | 21.         | 28.500      | 4.          |
| 12.700                 | 0.          | 16.700      | 852.        | 20.700      | 112.        | 24.700      | 20.         | 28.700      | 4.          |
| 12.900                 | 0.          | 16.900      | 696.        | 20.900      | 108.        | 24.900      | 18.         | 28.900      | 4.          |
| 13.100                 | 0.          | 17.100      | 573.        | 21.100      | 102.        | 25.100      | 17.         | 29.100      | 4.          |
| 13.300                 | 0.          | 17.300      | 490.        | 21.300      | 95.         | 25.300      | 15.         | 29.300      | 3.          |
| 13.500                 | 2.          | 17.500      | 442.        | 21.500      | 85.         | 25.500      | 14.         | 29.500      | 3.          |
| 13.700                 | 25.         | 17.700      | 422.        | 21.700      | 76.         | 25.700      | 12.         | 29.700      | 3.          |
| 13.900                 | 163.        | 17.900      | 415.        | 21.900      | 68.         | 25.900      | 11.         | 29.900      | 2.          |
| 14.100                 | 513.        | 18.100      | 406.        | 22.100      | 60.         | 26.100      | 11.         | 30.100      | 2.          |
| 14.300                 | 864.        | 18.300      | 385.        | 22.300      | 54.         | 26.300      | 10.         | 30.300      | 2.          |
| 14.500                 | 1251.       | 18.500      | 358.        | 22.500      | 49.         | 26.500      | 9.          | 30.500      | 2.          |
| 14.700                 | 1674.       | 18.700      | 328.        | 22.700      | 45.         | 26.700      | 9.          | 30.700      | 2.          |
| 14.900                 | 1937.       | 18.900      | 293.        | 22.900      | 41.         | 26.900      | 8.          | 30.900      | 2.          |
| 15.100                 | 2004.       | 19.100      | 255.        | 23.100      | 38.         | 27.100      | 7.          | 31.100      | 1.          |
| 15.300                 | 1957.       | 19.300      | 220.        | 23.300      | 35.         | 27.300      | 7.          | 31.300      | 1.          |
| 15.500                 | 1890.       | 19.500      | 189.        | 23.500      | 33.         | 27.500      | 6.          | 31.500      | 1.          |
| 15.700                 | 1765.       | 19.700      | 163.        | 23.700      | 30.         | 27.700      | 6.          | 31.700      | 1.          |
| 15.900                 | 1589.       | 19.900      | 143.        | 23.900      | 28.         | 27.900      | 5.          | 31.900      | 1.          |
| 16.100                 | 1398.       | 20.100      | 128.        | 24.100      | 26.         | 28.100      | 5.          |             |             |
| 16.300                 | 1214.       | 20.300      | 119.        | 24.300      | 23.         | 28.300      | 5.          |             |             |

RUNOFF VOLUME = 4.940 INCHES  
 PEAK DISCHARGE RATE = 2004.2 CFS



HYD NO=2

IDS OF HYDS TO BE ADDED ARE 1 AND 2

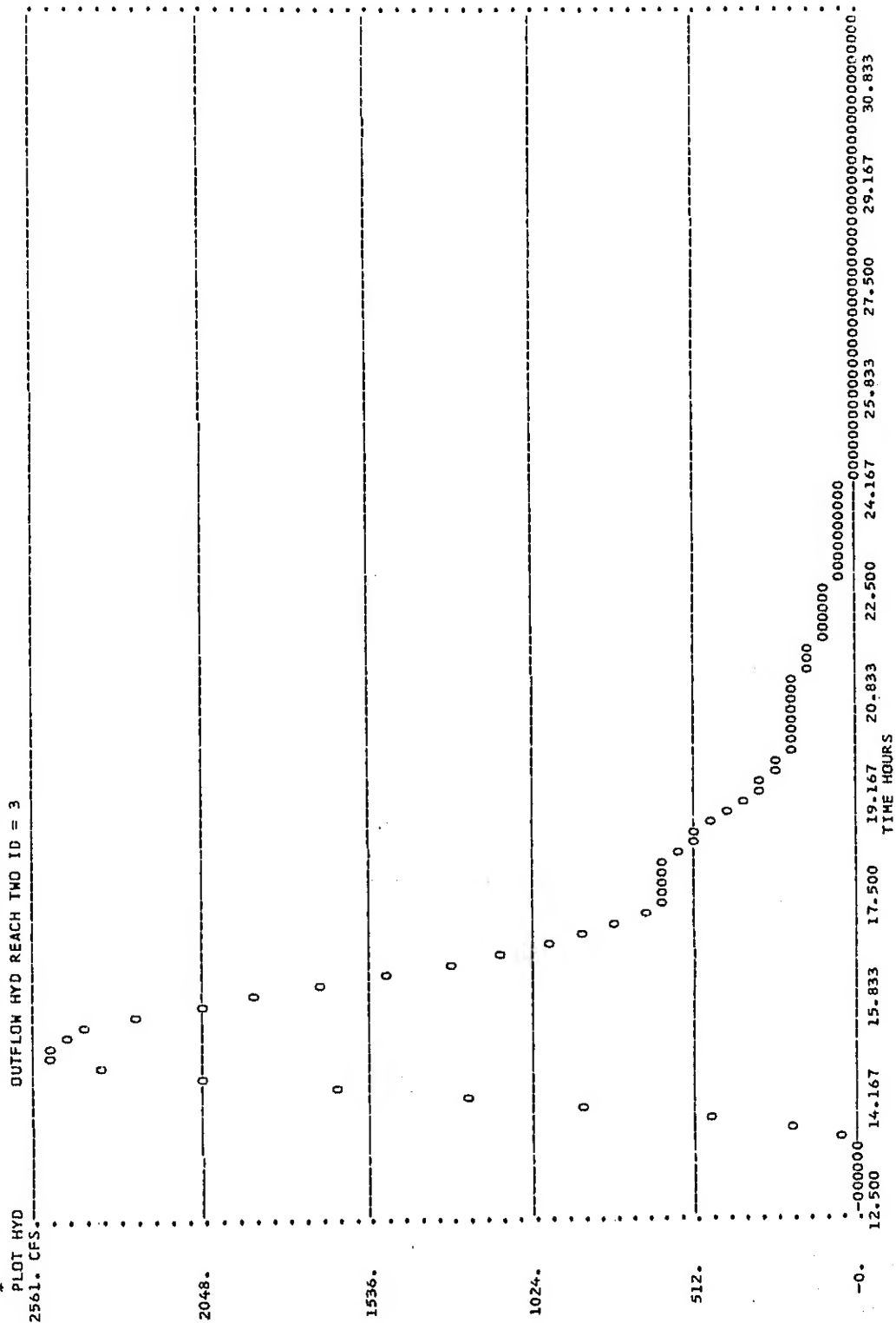
✻

## OUTFLOW HYDROGRAPH REACH 2

[illegible]

RUNOFF VOLUME = 4.674 INCHES  
PEAK DISCHARGE RATE = 2560.5 CFS

\* IT MAY BE DESIRABLE TO PLOT ALL HYDROGRAPHS. HOWEVER TO SAVE SPACE IN THIS \*  
 \* EXAMPLE, ONLY A FEW OUTFLOW HYDROGRAPHS ARE PLOTTED. \*



\* THIS COMPLETES THE ROUTING THROUGH THE FIRST REACH. FOR THE REMAINDER OF THE \*  
 \* ROUTING, COMMENTS AND KEYWORDS WILL BE BRIEFER.  
 \* VALLEY SECTIONS 5 6 AND 7 ARE USED TO ROUTE THROUGH REACH 3. THE RATING CURVE  
 \* HAS BEEN COMPUTED FOR VS 7 AND IS STORED IN ID 2. ID NUMBERS 1 AND 3 MUST BE  
 \* USED FOR VS-5 AND VS-6.

COMPUTE RATING CURVE ID=1 VS 6 3 SEG MIN ELEV=502.1 FT  
 MAX ELEV=511.0 FT CH SLP=.0018 FP SLP=.00245  
 N=.05 DIST=680 N=.103 DIST=695 N=.05 DIST=1025  

| DIST | ELEV  | DIST | ELEV  | DIST | ELEV  | DIST | ELEV  |
|------|-------|------|-------|------|-------|------|-------|
| 0    | 511.0 | 250  | 508.4 | 350  | 507.7 | 400  | 507.7 |
| 450  | 507.9 | 550  | 507.8 | 650  | 507.9 | 653  | 506.6 |
| 680  | 505.5 | 684  | 503.8 | 687  | 502.1 | 693  | 502.8 |
| 695  | 504.6 | 702  | 505.6 | 800  | 505.4 | 850  | 507.8 |
| 950  | 509.8 | 1025 | 511.0 |      |       |      |       |

# RATING CURVE VALLEY SECTION 6.0

| WATER<br>SURFACE<br>ELEV | AREA<br>SQ FT | FLOW<br>RATE<br>CFS |
|--------------------------|---------------|---------------------|
| 502.10                   | 0.0           | 0.0                 |
| 502.57                   | 1.1           | 0.9                 |
| 503.04                   | 4.3           | 6.2                 |
| 503.50                   | 8.3           | 16.8                |
| 503.97                   | 13.0          | 32.4                |
| 504.44                   | 18.4          | 53.4                |
| 504.91                   | 24.8          | 82.8                |
| 505.38                   | 33.3          | 122.0               |
| 505.85                   | 80.8          | 205.3               |
| 506.31                   | 150.3         | 373.0               |
| 506.78                   | 229.4         | 618.7               |
| 507.25                   | 314.4         | 946.0               |
| 507.72                   | 405.6         | 1303.6              |
| 508.19                   | 630.1         | 1826.8              |
| 508.66                   | 925.5         | 2672.5              |
| 509.12                   | 1254.0        | 3809.6              |
| 509.59                   | 1614.6        | 5249.7              |
| 510.06                   | 2007.6        | 6992.5              |
| 510.53                   | 2435.2        | 9076.7              |
| 511.00                   | 2897.5        | 11559.4             |

\*

COMPUTE RATING CURVE ID=3 VS 5 3 SEG MIN ELEV=496.6  
 MAX ELEV=506 FT CH SLP=-0018 FP SLP=-.00245  
 N=.05 DIST=314 N=-.03 DIST=326 N=.05 DIST=960  
 DIST ELEV DIST ELEV DIST ELEV DIST ELEV  
 25 506.0 150 503.7 200 502.2 250 501.2  
 300 502.5 314 500.5 317 497.5 320 496.6  
 325 496.9 326 500.5 334 501.3 350 502.0  
 400 503.4 450 503.8 550 503.7 650 504.1  
 800 505.4 850 504.5 900 505.4 950 506.0

RATING CURVE VALLEY SECTION 5.0

| WATER SURFACE ELEV | FLOW AREA SQ FT | FLOW RATE CFS |
|--------------------|-----------------|---------------|
| 496.60             | 0.0             | 0.0           |
| 497.09             | 2.1             | 2.1           |
| 497.59             | 5.9             | 9.9           |
| 498.08             | 10.1            | 23.1          |
| 498.58             | 14.7            | 41.0          |
| 499.07             | 19.6            | 63.3          |
| 499.57             | 24.8            | 90.2          |
| 500.06             | 30.3            | 121.8         |
| 500.56             | 36.1            | 159.5         |
| 501.05             | 44.6            | 215.3         |
| 501.55             | 62.9            | 287.4         |
| 502.04             | 108.9           | 403.4         |
| 502.54             | 184.6           | 592.3         |
| 503.03             | 282.2           | 887.2         |
| 503.52             | 397.5           | 1272.9        |
| 504.02             | 583.1           | 1723.6        |
| 504.51             | 854.7           | 2526.8        |
| 505.01             | 1182.7          | 3561.5        |
| 505.50             | 1578.6          | 4956.2        |
| 506.00             | 2022.1          | 6825.7        |



COMPUTE TRAVEL TIME ID=1 REACH 3 3 VS LENGTH=3330 FT SLP=-.00245 \*

TRAVEL TIME TABLE  
REACH 3-0

| ROUTE | ID=1 | HYD NO=102 | INFLOW ID=3 | DT=.2 HR | WATER<br>DEPTH<br>FEET | FLOW<br>RATE<br>CFS | TRAVEL<br>TIME<br>HRS |
|-------|------|------------|-------------|----------|------------------------|---------------------|-----------------------|
|       |      |            |             |          | 0.45                   | 2.                  | 0.8623                |
|       |      |            |             |          | 0.96                   | 10.                 | 0.5484                |
|       |      |            |             |          | 1.45                   | 23.                 | 0.4135                |
|       |      |            |             |          | 1.92                   | 41.                 | 0.3434                |
|       |      |            |             |          | 2.37                   | 63.                 | 0.2988                |
|       |      |            |             |          | 2.80                   | 90.                 | 0.2674                |
|       |      |            |             |          | 3.22                   | 122.                | 0.2447                |
|       |      |            |             |          | 3.58                   | 160.                | 0.2527                |
|       |      |            |             |          | 3.99                   | 215.                | 0.2703                |
|       |      |            |             |          | 4.32                   | 287.                | 0.2906                |
|       |      |            |             |          | 4.69                   | 403.                | 0.3160                |
|       |      |            |             |          | 5.10                   | 592.                | 0.3241                |
|       |      |            |             |          | 5.57                   | 887.                | 0.3265                |
|       |      |            |             |          | 6.03                   | 1273.               | 0.3205                |
|       |      |            |             |          | 6.45                   | 1724.               | 0.3371                |
|       |      |            |             |          | 6.91                   | 2527.               | 0.3349                |
|       |      |            |             |          | 7.40                   | 3561.               | 0.3331                |
|       |      |            |             |          | 7.86                   | 4956.               | 0.3286                |
|       |      |            |             |          | 8.31                   | 6826.               | 0.3039                |

\* IT MAY NOT BE NECESSARY TO PRINT THE COORDINATES OF ALL HYDS. FOR THE  
\* REMAINDER OF THE EXAMPLE, ONLY REACH OUTFLOW HYDS WILL BE PRINTED. TO PRINT  
\* ONLY THE RUNOFF VOLUME AND PEAK RATE, A CODE IS USED WITH PRINT HYD.

PRINT HYD ID=1 CODE=1

PARTIAL HYDROGRAPH 102

RUNOFF VOLUME = 4.672 INCHES  
PEAK DISCHARGE RATE = 2366.2 CFS

\* COMPUTE THE HYD FROM AREA 303.

\* COMPUTE HYD ID=2 HYD NO 303 DT=.1666667 HR DA=1.108 50 MI CN=82  
HT=80 FT L=1.7 MI CODE=-1 (SIGNAL TO USE SAME MASS  
RAINFALL AS USED IN PREVIOUS HYD)  
SHAPE CONSTANT, N = 2.248  
UNIT PEAK = 253.1CFS

PRINT HYD ID=2 CODE=1

HYDROGRAPH FROM AREA 303

RUNOFF VOLUME = 4.131 INCHES  
PEAK DISCHARGE RATE = 673.5 CFS

\* \* TO OBTAIN THE OUTFLOW FROM REACH 3, ADD HYD FROM AREA 303 TO ROUTED HYD 102.\*

ADD HYD ID=3 HYD NO=3 IDS ADDED ARE 1 AND 2  
PRINT HYD ID=3

| OUTFLOW HYDROGRAPH REACH 3 |             |             |             |             |             |             |             |             |             |
|----------------------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| TIME<br>HRS                | FLOW<br>CFS | TIME<br>HRS | FLOW<br>CFS | TIME<br>HRS | FLOW<br>CFS | TIME<br>HRS | FLOW<br>CFS | TIME<br>HRS | FLOW<br>CFS |
| 12.500                     | 0.          | 18.333      | 918.        | 24.166      | 112.        | 29.999      | 24.         | 35.832      | 2.          |
| 12.667                     | 0.          | 18.500      | 883.        | 24.333      | 105.        | 30.166      | 23.         | 35.999      | 2.          |
| 12.833                     | 0.          | 18.666      | 839.        | 24.499      | 100.        | 30.332      | 22.         | 36.165      | 2.          |
| 13.000                     | 0.          | 18.833      | 789.        | 24.666      | 94.         | 30.499      | 20.         | 36.332      | 1.          |
| 13.167                     | 1.          | 19.000      | 736.        | 24.833      | 90.         | 30.666      | 19.         | 36.499      | 1.          |
| 13.333                     | 3.          | 19.166      | 680.        | 24.999      | 86.         | 30.832      | 18.         | 36.665      | 1.          |
| 13.500                     | 10.         | 19.333      | 626.        | 25.166      | 82.         | 30.999      | 17.         | 36.832      | 1.          |
| 13.667                     | 48.         | 19.500      | 574.        | 25.333      | 78.         | 31.166      | 16.         | 36.999      | 1.          |
| 13.833                     | 172.        | 19.666      | 526.        | 25.499      | 74.         | 31.332      | 15.         | 37.165      | 1.          |
| 14.000                     | 398.        | 19.833      | 485.        | 25.666      | 71.         | 31.499      | 15.         | 37.332      | 1.          |
| 14.167                     | 692.        | 20.000      | 449.        | 25.833      | 67.         | 31.666      | 14.         | 37.499      | 1.          |
| 14.333                     | 1028.       | 20.166      | 419.        | 25.999      | 64.         | 31.832      | 13.         | 37.665      | 1.          |
| 14.500                     | 1432.       | 20.333      | 391.        | 26.166      | 62.         | 31.999      | 13.         | 37.832      | 0.          |
| 14.667                     | 1877.       | 20.500      | 374.        | 26.333      | 59.         | 32.166      | 12.         | 37.999      | 0.          |
| 14.833                     | 2288.       | 20.666      | 355.        | 26.499      | 57.         | 32.332      | 11.         | 38.165      | 0.          |
| 15.000                     | 2615.       | 20.833      | 335.        | 26.666      | 55.         | 32.499      | 11.         | 38.332      | 0.          |
| 15.167                     | 2848.       | 21.000      | 315.        | 26.833      | 53.         | 32.666      | 10.         | 38.499      | 0.          |
| 15.333                     | 2984.       | 21.166      | 294.        | 26.999      | 50.         | 32.832      | 10.         | 38.665      | 0.          |
| 15.500                     | 3027.       | 21.333      | 277.        | 27.166      | 48.         | 32.999      | 9.          | 38.832      | 0.          |
| 15.667                     | 2977.       | 21.500      | 258.        | 27.333      | 46.         | 33.166      | 9.          | 38.999      | 0.          |
| 15.833                     | 2864.       | 21.666      | 235.        | 27.499      | 44.         | 33.332      | 9.          | 39.165      | 0.          |
| 16.000                     | 2704.       | 21.833      | 215.        | 27.666      | 42.         | 33.499      | 8.          | 39.332      | 0.          |
| 16.167                     | 2515.       | 22.000      | 200.        | 27.833      | 40.         | 33.666      | 8.          | 39.499      | 0.          |
| 16.333                     | 2315.       | 22.166      | 186.        | 27.999      | 39.         | 33.832      | 7.          | 39.665      | 0.          |
| 16.500                     | 2119.       | 22.333      | 173.        | 28.166      | 37.         | 33.999      | 6.          | 39.832      | 0.          |
| 16.667                     | 1927.       | 22.500      | 161.        | 28.333      | 36.         | 34.166      | 6.          | 39.999      | 0.          |
| 16.833                     | 1738.       | 22.666      | 151.        | 28.499      | 34.         | 34.332      | 5.          | 40.165      | 0.          |
| 17.000                     | 1553.       | 22.833      | 142.        | 28.666      | 33.         | 34.499      | 4.          | 40.332      | 0.          |
| 17.167                     | 1380.       | 23.000      | 133.        | 28.833      | 32.         | 34.666      | 4.          | 40.498      | 0.          |
| 17.333                     | 1226.       | 23.166      | 126.        | 28.999      | 31.         | 34.832      | 3.          | 40.665      | 0.          |
| 17.500                     | 1104.       | 23.333      | 118.        | 29.166      | 30.         | 34.999      | 2.          | 40.832      | 0.          |
| 17.667                     | 1028.       | 23.500      | 110.        | 29.333      | 28.         | 35.165      | 2.          | 40.998      | 0.          |
| 17.833                     | 994.        | 23.666      | 104.        | 29.499      | 27.         | 35.332      | 2.          | 41.165      | 0.          |
| 18.000                     | 970.        | 23.833      | 100.        | 29.666      | 26.         | 35.499      | 2.          | 41.332      | 0.          |
| 18.167                     | 947.        | 23.999      | 118.        | 29.832      | 25.         | 35.665      | 2.          |             |             |

RUNOFF VOLUME = 4.509 INCHES  
PEAK DISCHARGE RATE = 3026.6 CFS

\* ROUTE THROUGH REACH 4.

\* COMPUTE RATING CURVE ID=1 VS=4 3 SEG MIN ELEV 491.8  
 MAX ELEV=501.8 CH SLP=.0018 FP SLP=.003  
 N=.05 DIST=1046 N=-.03 DIST=1068 N=.05 DIST=1082  
 DIST ELEV DIST ELEV DIST ELEV DIST ELEV  
 0 501.0 200 500.3 250 500.3 300 499.9  
 450 499.1 500 500.8 550 498.9 600 499.0  
 700 499.5 800 499.6 850 499.0 900 497.7  
 950 497.6 1000 497.1 1031 497.4 1046 497.2  
 1050 494.5 1056 494.2 1061 491.9 1064 491.8  
 1068 495.7 1072 497.4 1082 501.0

RATING CURVE VALLEY SECTION 4.0

| WATER<br>SURFACE<br>ELEV | AREA<br>SQ FT | FLOW<br>RATE<br>CFS |
|--------------------------|---------------|---------------------|
| 491.80                   | 0.0           | 0.0                 |
| 492.28                   | 1.6           | 1.7                 |
| 492.77                   | 4.1           | 6.6                 |
| 493.25                   | 7.3           | 15.1                |
| 493.74                   | 11.2          | 27.8                |
| 494.22                   | 16.0          | 44.6                |
| 494.70                   | 23.3          | 62.5                |
| 495.19                   | 32.0          | 103.5               |
| 495.67                   | 41.2          | 155.2               |
| 496.16                   | 51.2          | 222.8               |
| 496.64                   | 62.1          | 305.1               |
| 497.13                   | 73.9          | 403.4               |
| 497.61                   | 115.2         | 553.8               |
| 498.09                   | 200.0         | 813.9               |
| 498.58                   | 296.4         | 1195.6              |
| 499.06                   | 408.8         | 1598.0              |
| 499.55                   | 612.3         | 2078.4              |
| 500.03                   | 949.7         | 3122.3              |
| 500.51                   | 1350.0        | 4498.2              |
| 501.00                   | 1837.5        | 6404.5              |

COMPUTE RATING CURVE ID=2 VS=3 3 SEG MIN ELEV=486.2  
 MAX ELEV=499 CH SLP=.0018 FP SLP=.0036  
 N=.05 DIST=520 N=-.03 DIST=547 N=.05 DIST=1200  
 DIST ELEV DIST ELEV DIST ELEV DIST ELEV  
 297 499.0 350 496.4 378 494.7 400 491.7  
 450 491.8 500 492.2 520 491.2 529 486.6  
 536 486.2 540 490.4 547 492.7 600 495.9  
 650 496.1 729 496.7 900 496.6 1000 497.0  
 1150 498.3 1210 499.0

RATING CURVE VALLEY SECTION 3.0

| WATER<br>SURFACE<br>ELEV | FLOW<br>AREA<br>SQ FT | FLOW<br>RATE<br>CFS |
|--------------------------|-----------------------|---------------------|
| 486.20                   | 0.0                   | 0.0                 |
| 486.87                   | 3.6                   | 4.4                 |
| 487.55                   | 9.8                   | 20.6                |
| 488.22                   | 17.3                  | 48.2                |
| 488.89                   | 26.1                  | 88.8                |
| 489.57                   | 36.2                  | 144.3               |
| 490.24                   | 47.6                  | 217.0               |
| 490.92                   | 60.7                  | 300.6               |
| 491.59                   | 77.3                  | 419.1               |
| 492.26                   | 143.6                 | 626.6               |
| 492.94                   | 247.2                 | 1054.5              |
| 493.61                   | 360.4                 | 1720.5              |
| 494.28                   | 484.4                 | 2616.8              |
| 494.96                   | 619.5                 | 3756.2              |
| 495.63                   | 768.9                 | 5163.4              |
| 496.30                   | 949.8                 | 6844.7              |
| 496.98                   | 1271.9                | 9049.4              |
| 497.65                   | 1746.6                | 12457.3             |
| 498.32                   | 2283.0                | 17061.9             |
| 499.00                   | 2873.8                | 23295.3             |

COMPUTE TRAVEL TIME ID=1 REACH 4 3 VS L=3415 SLP=-.003 \*

TRAVEL TIME TABLE  
REACH 4.0

| WATER<br>DEPTH<br>FEET | FLOW<br>RATE<br>CFS | TRAVEL<br>TIME<br>HRS |
|------------------------|---------------------|-----------------------|
| 0.38                   | 2.                  | 0.8777                |
| 0.84                   | 7.                  | 0.6140                |
| 1.25                   | 15.                 | 0.4719                |
| 1.69                   | 28.                 | 0.3899                |
| 2.14                   | 45.                 | 0.3386                |
| 2.54                   | 62.                 | 0.3192                |
| 3.15                   | 104.                | 0.2683                |
| 3.75                   | 155.                | 0.2335                |
| 4.32                   | 223.                | 0.2076                |
| 4.87                   | 305.                | 0.2004                |
| 5.36                   | 403.                | 0.2022                |
| 5.82                   | 554.                | 0.2311                |
| 6.32                   | 814.                | 0.2513                |
| 6.83                   | 1196.               | 0.2491                |
| 7.28                   | 1598.               | 0.2532                |
| 7.69                   | 2078.               | 0.2625                |
| 8.27                   | 3122.               | 0.2570                |
| 8.86                   | 4498.               | 0.2458                |
| 9.47                   | 6405.               | 0.2302                |

ROUTE ID=1 HYD NO=103 INFLOW ID=3 DT=.2  
PRINT HYD ID=1 CODE=1

PARTIAL HYDROGRAPH 103

RUNOFF VOLUME = 4.508 INCHES  
PEAK DISCHARGE RATE = 2904.3 CFS

\* COMPUTE THE HYD FROM AREA 304.

\*  
COMPUTE HYD ID=2 HYD NO=304 DT=.25 DA=.807 CN=82  
HT=80 L=1.70  
RAINFALL = 0 0 .45 .59 .87 1.7 2.72 3.35 3.98 4.65 4.8 4.98  
5.07 5.07 5.07 5.11 5.21 5.34 5.34 5.35 5.45 5.77 5.88 5.95  
6.06 6.1 6.1 6.1 6.11 6.11 6.11 6.12 6.12 6.12 6.12 6.13  
6.13 6.13 6.13 6.14 6.17 6.17 6.17 6.17 6.17 6.18 6.18 6.19  
SHAPE CONSTANT, N = 2.156  
UNIT PEAK = 192.9CFS

PRINT HYD ID=2 CODE=1

HYDROGRAPH FROM AREA 304

RUNOFF VOLUME = 4.111 INCHES  
PEAK DISCHARGE RATE = 504.5 CFS

\* ADC HYD  
PRINT HYD

ID=3 HYD NO=4 ICS AGED ARE 1 AND 2  
ID=3

OUTFLOW-HYDROGRAPH REACH 4

[illegible]

RUNOFF VOLUME = 4.436 INCHES  
PEAK DISCHARGE RATE = 3351.1 CFS

\* ROUTE THROUGH REACH 5.

\* COMPUTE RATING CURVE ID=1 VS 2 3 SEG MIN ELEV=481.8  
 MAX ELEV 493 CH SLP=.0018 FP SLP=.0036  
 N=.05 DIST=387 N=.03 DIST=405 N=.05 DIST=558  
 DIST ELEV DIST ELEV DIST ELEV DIST ELEV  
 131 493.0 150 492.0 189 490.8 250 490.6  
 258 489.9 270 486.8 300 485.5 350 485.9  
 387 485.5 392 483.3 397 482.1 400 481.8  
 405 485.4 427 488.6 450 490.1 550 492.9  
 558 493.0

RATING CURVE VALLEY SECTION 2-0

| WATER SURFACE ELEV | AREA SQ FT | FLOW CFS | FLOW RATE CFS |
|--------------------|------------|----------|---------------|
| 481.80             | 0.0        | 0.0      | 0.0           |
| 482.39             | 1.7        | 1.8      | 1.8           |
| 482.98             | 5.7        | 9.4      | 9.4           |
| 483.57             | 11.4       | 25.6     | 25.6          |
| 484.16             | 18.6       | 52.2     | 52.2          |
| 484.75             | 27.0       | 90.1     | 90.1          |
| 485.34             | 36.7       | 141.1    | 141.1         |
| 485.93             | 69.9       | 237.2    | 237.2         |
| 486.51             | 144.9      | 461.2    | 461.2         |
| 487.10             | 229.5      | 818.5    | 818.5         |
| 487.69             | 318.5      | 1316.9   | 1316.9        |
| 488.28             | 411.3      | 1958.3   | 1958.3        |
| 488.87             | 508.1      | 2749.5   | 2749.5        |
| 489.46             | 611.1      | 3713.2   | 3713.2        |
| 490.05             | 720.9      | 4861.2   | 4861.2        |
| 490.64             | 842.5      | 5879.6   | 5879.6        |
| 491.23             | 1013.0     | 6693.6   | 6693.6        |
| 491.82             | 1210.7     | 8589.4   | 8589.4        |
| 492.41             | 1430.9     | 11066.8  | 11066.8       |
| 493.00             | 1670.6     | 14198.7  | 14198.7       |

COMPUTE RATING CURVE ID=3 VS=1 3 SEG MIN ELEV=474.1 MAX ELEV=488  
 CH SLP=-.0018 FP SLP=-.0028 N=.05 DIST= 232  
 N=-.03 DIST= 250 N=.05 DIST= 627  

| DIST | ELEV  | DIST | ELEV  | DIST | ELEV  |
|------|-------|------|-------|------|-------|
| 61   | 488.0 | 100  | 486.6 | 171  | 481.0 |
| 232  | 478.6 | 236  | 474.2 | 242  | 474.1 |
| 250  | 478.9 | 300  | 482.9 | 350  | 484.2 |
| 627  | 488.0 |      |       | 400  | 484.2 |

RATING CURVE VALLEY SECTION 1.0  

| WATER<br>SURFACE<br>ELEV | WATER<br>AREA<br>SQ FT | FLOW<br>RATE<br>CFS |
|--------------------------|------------------------|---------------------|
| 474.10                   | 0.0                    | 0.0                 |
| 474.83                   | 4.6                    | 7.0                 |
| 475.56                   | 10.7                   | 25.4                |
| 476.29                   | 18.0                   | 55.1                |
| 477.03                   | 26.5                   | 97.4                |
| 477.76                   | 36.2                   | 154.2               |
| 478.49                   | 47.4                   | 220.9               |
| 479.22                   | 62.4                   | 331.5               |
| 479.95                   | 87.4                   | 507.9               |
| 480.68                   | 123.2                  | 756.2               |
| 481.41                   | 192.1                  | 1108.7              |
| 482.15                   | 283.5                  | 1659.7              |
| 482.88                   | 388.3                  | 2411.3              |
| 483.61                   | 513.1                  | 3352.4              |
| 484.34                   | 672.5                  | 4507.0              |
| 485.07                   | 896.5                  | 6323.3              |
| 485.80                   | 1159.2                 | 8782.5              |
| 486.53                   | 1460.7                 | 12141.1             |
| 487.27                   | 1804.2                 | 16663.6             |
| 488.00                   | 2194.6                 | 23601.4             |



COMPUTE TRAVEL TIME ID=1 REACH 5 3 VS L=3310 SLP=.003

TRAVEL TIME TABLE  
REACH 5.0

| WATER<br>DEPTH<br>FEET | FLOW<br>RATE<br>CFS | TRAVEL<br>TIME<br>MRS |
|------------------------|---------------------|-----------------------|
| 0.35                   | 2.                  | 0.7488                |
| 0.96                   | 9.                  | 0.5416                |
| 1.57                   | 26.                 | 0.3996                |
| 2.19                   | 52.                 | 0.3173                |
| 2.82                   | 90.                 | 0.2666                |
| 3.45                   | 141.                | 0.2309                |
| 4.28                   | 237.                | 0.2201                |
| 5.30                   | 461.                | 0.2103                |
| 6.13                   | 818.                | 0.2078                |
| 6.83                   | 1317.               | 0.1948                |
| 7.47                   | 1958.               | 0.1768                |
| 8.09                   | 2750.               | 0.1607                |
| 8.71                   | 3713.               | 0.1476                |
| 9.31                   | 4861.               | 0.1371                |
| 9.78                   | 5880.               | 0.1319                |
| 10.18                  | 6694.               | 0.1320                |
| 10.77                  | 8589.               | 0.1268                |
| 11.33                  | 11067.              | 0.1204                |
| 11.89                  | 14199.              | 0.1130                |

ROUTE ID=1 HYD NO=104 INFLOW ID=3 DT=.2  
PRINT HYD ID=1 CODE=1

PARTIAL HYDROGRAPH 104

RUNOFF VOLUME = 4.436 INCHES  
PEAK DISCHARGE RATE = 3318.5 CFS

COMPUTE HYD ID=2 HYD NO=305 DT=.333333 DA=1.875 CN=82  
K=-2 TP=-1.2  
RAINFALL 0 0 .29 .61 1.12 2.27 3.24 4.21 4.76 4.94 5.03  
5.03 5.07 5.31 5.43 5.44 5.5 5.7 5.71 5.71 5.72 5.7  
5.73 5.78 5.79 5.8 5.8 5.81 5.83 5.84 5.85 5.85 5.  
5.87  
SHAPE CONSTANT, N = - 2.254  
UNIT PEAK = 334.3CFS

PRINT HYD ID=2 CODE=1

HYDROGRAPH FROM AREA 305

RUNOFF VOLUME = 3.837 INCHES  
PEAK DISCHARGE RATE = 936.7 CFS

```

* ADD THE HYD FROM AREA 305 TO THE PARTIAL HYD 104.
*
ADC HYD      ID=3  HYD NO=105  IDS ADDED ARE 1 AND 2
PRINT HYD    ID=3  CODE=1

PARTIAL HYDROGRAPH 105

RUNOFF VOLUME = 4.259 INCHES
PEAK DISCHARGE RATE = 4244.3 CFS

* THE HYD FROM AREA 306 WAS MEASURED, SO STORE HYD IS USED TO STORE IT IN THE
* PROGRAM.
*
STORE HYD
ID=1  HYD NO=306  DT=.25  DA=.483
FLOW RATE CFS= 0 0 0 45 280 560 638 570 370 258 170 97 72
64 61 80 70 59 54 52 51 50 46 44 40 38 33 30 27 25 24 23 22
21 20 20 19 18 16 15 13 11 10 9 8 7 6 5 5 4 4 3 3 3 2
2 2 1 1

* ROUTE THE HYD FROM AREA 306 THROUGH REACH 6.
*
COMPUTE RATING CURVE ID=1  VS=21  3 SEG  MIN ELEV=506.0  MAX ELEV=514
CH SLP= .006  FP SLP= .0075  N=.05  DIST= 300
N=-.03  DIST= 310  N=.05  DIST= 570
DIST  ELEV  DIST  ELEV  DIST  ELEV  DIST  ELEV
0  514.0  300  508.0  302  506.0  307  506.0
310  508.0  380  510.0  520  512.0  570  514.0

RATING CURVE VALLEY SECTION 21.0
WATER SURFACE AREA FLOW FLOW
ELEV SQ FT RATE CFS
506.00 0.0 0.0
506.42 2.3 4.7
506.84 5.1 15.7
507.26 8.3 32.6
507.68 12.0 55.7
508.10 16.5 87.5
508.53 32.0 146.0
508.95 62.5 250.6
509.37 108.1 420.9
509.79 168.8 675.2
510.21 245.2 1018.8
510.63 342.2 1482.0
511.05 460.4 2102.0
511.47 599.9 2902.4
511.89 760.6 3907.9
512.31 940.3 5214.1
512.73 1133.7 6796.0
513.16 1340.3 8649.2
513.58 1560.2 10795.8
514.00 1793.3 13260.7

```

COMPUTE RATING CURVE ID=2 VS=20 3 SEG MIN ELEV=482.0 MAX ELEV=492.0  
 CH SLP=.006 FP SLP=.0075 N=.05 DIST=175  
 N=-.03 DIST=205 N=.05 DIST=450

| DIST | ELEV  | DIST | ELEV  | DIST | ELEV  | DIST | ELEV  |
|------|-------|------|-------|------|-------|------|-------|
| 0    | 492.0 | 100  | 490.0 | 175  | 484.0 | 188  | 482.0 |
| 190  | 482.0 | 205  | 484.0 | 250  | 486.0 | 275  | 488.0 |
| 310  | 490.0 | 450  | 492.0 |      |       |      |       |

RATING CURVE VALLEY SECTION 20.0

| WATER SURFACE ELEV | FLOW AREA SQ FT | FLOW RATE CFS |
|--------------------|-----------------|---------------|
| 482.00             | 0.0             | 0.0           |
| 482.53             | 3.0             | 5.5           |
| 483.05             | 9.9             | 27.8          |
| 483.58             | 20.6            | 76.1          |
| 484.10             | 35.3            | 164.8         |
| 484.63             | 57.9            | 329.7         |
| 485.16             | 90.1            | 573.6         |
| 485.68             | 132.0           | 917.0         |
| 486.21             | 183.4           | 1384.8        |
| 486.74             | 242.3           | 1999.6        |
| 487.26             | 308.0           | 2777.3        |
| 487.79             | 380.7           | 3744.8        |
| 488.31             | 460.5           | 4921.7        |
| 488.84             | 548.5           | 6356.6        |
| 489.37             | 644.8           | 8115.9        |
| 489.89             | 749.5           | 10274.9       |
| 490.42             | 870.3           | 12413.3       |
| 490.94             | 1023.7          | 15306.2       |
| 491.47             | 1210.4          | 19275.9       |
| 492.00             | 1430.4          | 24694.0       |

\*

COMPUTE TRAVEL TIME ID=2 REACH 6 2 VS L=4080 SLP=.0075

TRAVEL TIME TABLE  
REACH 6.0

| ROUTE<br>PRINT | HYD | ID=2 | HYD NO=106 | ID=2 | CODE=1 | INFLW | ID=1   | DT=.2  | TRAVEL TIME            |                     |                       |
|----------------|-----|------|------------|------|--------|-------|--------|--------|------------------------|---------------------|-----------------------|
|                |     |      |            |      |        |       |        |        | WATER<br>DEPTH<br>FEET | FLOW<br>RATE<br>CFS | TRAVEL<br>TIME<br>HRS |
|                |     |      |            |      |        | 0.44  | 5.     | 0.5893 | 0.80                   | 16.                 | 0.4055                |
|                |     |      |            |      |        | 1.18  | 33.    | 0.3346 | 1.52                   | 56.                 | 0.2852                |
|                |     |      |            |      |        | 1.88  | 88.    | 0.2525 | 2.26                   | 146.                | 0.2491                |
|                |     |      |            |      |        | 2.66  | 251.   | 0.2478 | 3.10                   | 421.                | 0.2397                |
|                |     |      |            |      |        | 3.55  | 675.   | 0.2277 | 4.00                   | 1019.               | 0.2161                |
|                |     |      |            |      |        | 4.46  | 1482.  | 0.2045 | 4.93                   | 2102.               | 0.1918                |
|                |     |      |            |      |        | 5.40  | 2902.  | 0.1791 | 5.88                   | 3908.               | 0.1671                |
|                |     |      |            |      |        | 6.37  | 5214.  | 0.1542 | 6.85                   | 6796.               | 0.1423                |
|                |     |      |            |      |        | 7.33  | 8649.  | 0.1318 | 7.80                   | 10796.              | 0.1228                |
|                |     |      |            |      |        | 8.28  | 13261. | 0.1157 |                        |                     |                       |

PARTIAL HYDROGRAPH 106

RUNOFF VOLUME = 3.364 INCHES  
PEAK DISCHARGE RATE = 574.6 CFS

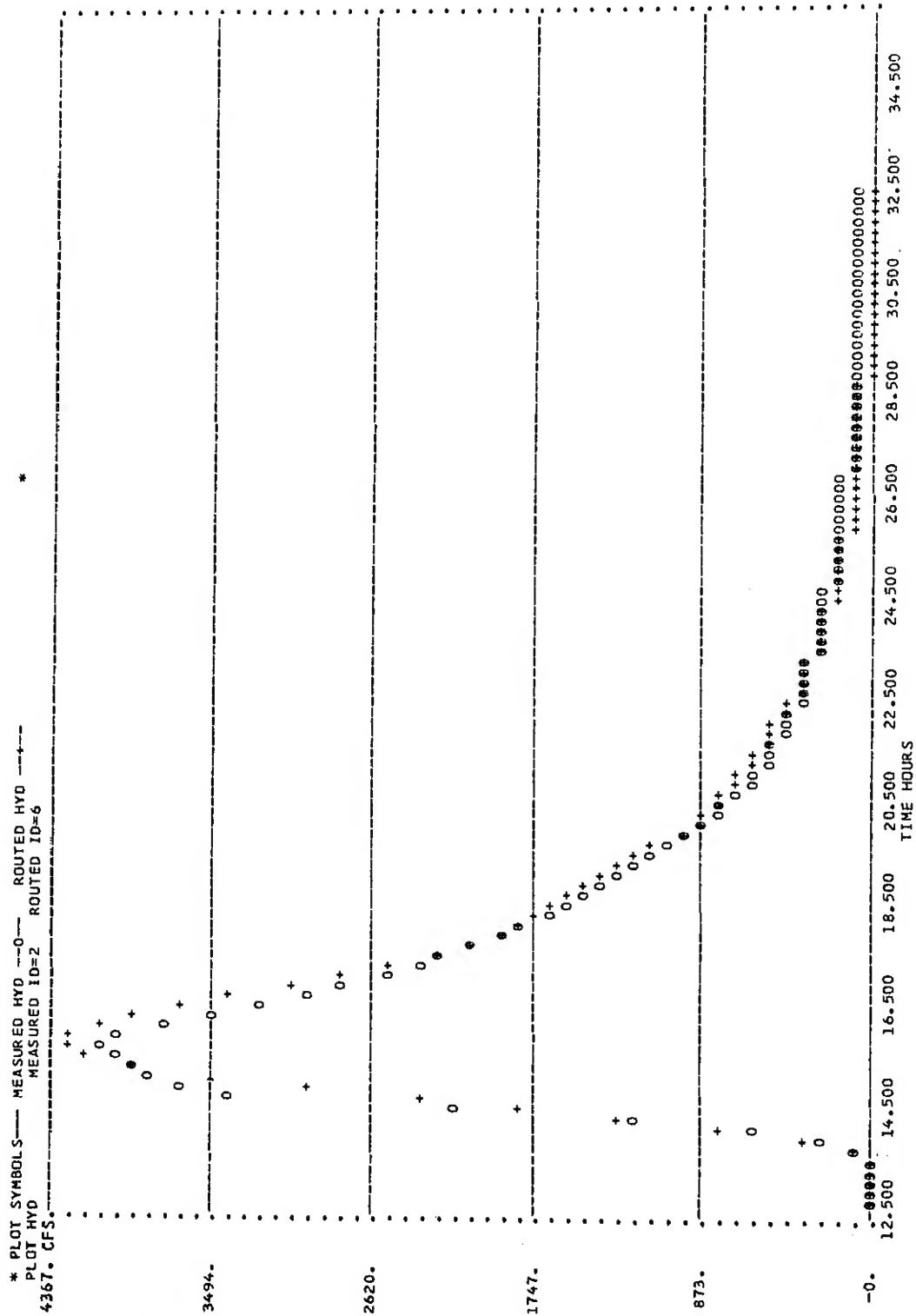
OUTFLOW HYDROGRAPH REACH 5

RUNOFF VOLUME = 4.196 INCHES  
PEAK DISCHARGE RATE = 4367.5 CFS

```

* THE SEDIMENT YIELD COMMAND IS USED TO COMPUTE THE SEDIMENT YIELD PRODUCED BY *
* THE ROUTED FLOOD.
*
SEDIMENT YIELD ID=6 SOIL=.34 CROP=.16 CP=.4 LS=.3
SEDIMENT YIELD = 4116.9 TONS
* THE MEASURED SEDIMENT YIELD FOR THIS FLOOD WAS 3916 TONS.
* THE ROUTED OUTFLOW HYDROGRAPH CAN BE COMPARED WITH THE MEASURED HYDROGRAPH BY
* PLOTTING AND ERROR ANALYSIS
*
* STORE THE MEASURED HYDROGRAPH
*
STORE HYD
ID=2 HYD NO=5 DI=-.1666667 DA=6.84
FLOW RATE = 0 0 0 0 100 220 400 790 1350 2200 3400
3650 3800 3920 4020 4190 4260 4100 3910 3700 3500 3280 3070
2860 2700 2550 2400 2290 2150 2000 1900 1800 1700 1620 1530
1460 1380 1300 1210 1150 1090 1030 970 900 820 800 750 700
670 620 600 570 530 510 500 490 470 430 400 390 380 370 350
340 330 320 310 300 300 290 270 260 240 220 210 210 200 200
200 190 190 190 180 180 170 170 160 160 160 150 150 150 150
150 150 140 140 140 140 140 140 140 140 130 120 120 120 120
120 110 110 110 110 110 110 110 110 100 100 90

```



\* THE ERROR ANALYSIS COMMAND IS USED TO COMPUTE THE MAGNITUDE OF THE ERROR \*

ERROR ANALYSIS MEASURED ID=2 (FLOW ONE) ROUTED ID=6 (FLOW TWO)

| TIME<br>HRS | FLOW 1<br>CFS | FLOW 2<br>CFS | ERROR<br>CFS |
|-------------|---------------|---------------|--------------|
| 12.500      | 0.            | 0.            | 0.           |
| 12.700      | 0.            | 0.            | -0.          |
| 12.900      | 0.            | 0.            | -0.          |
| 13.100      | 0.            | 0.            | -0.          |
| 13.300      | 0.            | 3.            | -3.          |
| 13.500      | 0.            | 15.           | -15.         |
| 13.700      | 124.          | 106.          | 18.          |
| 13.900      | 292.          | 378.          | -86.         |
| 14.100      | 634.          | 829.          | -195.        |
| 14.300      | 1238.         | 1349.         | -111.        |
| 14.500      | 2230.         | 1855.         | 345.         |
| 14.700      | 3450.         | 2403.         | 1047.        |
| 14.900      | 3710.         | 2983.         | 727.         |
| 15.100      | 3872.         | 3537.         | 335.         |
| 15.300      | 4000.         | 3968.         | 32.          |
| 15.500      | 4100.         | 4260.         | -160.        |
| 15.700      | 4180.         | 4367.         | -187.        |
| 15.900      | 4024.         | 4337.         | -313.        |
| 16.100      | 3784.         | 4181.         | -397.        |
| 16.300      | 3540.         | 3950.         | -410.        |
| 16.500      | 3280.         | 3684.         | -404.        |
| 16.700      | 3028.         | 3415.         | -387.        |
| 16.900      | 2796.         | 3143.         | -347.        |
| 17.100      | 2610.         | 2880.         | -270.        |
| 17.300      | 2430.         | 2611.         | -181.        |
| 17.500      | 2290.         | 2353.         | -63.         |
| 17.700      | 2120.         | 2137.         | -17.         |
| 17.900      | 1960.         | 1978.         | -18.         |
| 18.100      | 1940.         | 1869.         | -29.         |
| 18.300      | 1720.         | 1783.         | -63.         |
| 18.500      | 1620.         | 1707.         | -87.         |
| 18.700      | 1516.         | 1628.         | -112.        |
| 18.900      | 1428.         | 1541.         | -113.        |
| 19.100      | 1332.         | 1446.         | -114.        |
| 19.300      | 1228.         | 1347.         | -119.        |
| 19.500      | 1150.         | 1244.         | -94.         |
| 19.700      | 1072.         | 1141.         | -69.         |
| 19.900      | 988.          | 1044.         | -56.         |
| 20.100      | 928.          | 959.          | -31.         |
| 20.300      | 836.          | 889.          | -51.         |
| 20.500      | 800.          | 833.          | -33.         |
| 20.700      | 740.          | 788.          | -48.         |
| 20.900      | 688.          | 749.          | -61.         |
| 21.100      | 640.          | 714.          | -74.         |
| 21.300      | 604.          | 678.          | -74.         |
| 21.500      | 570.          | 641.          | -71.         |
| 21.700      | 526.          | 604.          | -78.         |
| 21.900      | 506.          | 568.          | -62.         |
| 22.100      | 494.          | 532.          | -38.         |
| 22.300      | 474.          | 497.          | -23.         |
| 22.500      | 430.          | 466.          | -36.         |
| 22.700      | 398.          | 436.          | -38.         |
| 22.900      | 386.          | 407.          | -21.         |



|        |      |      |     |
|--------|------|------|-----|
| 23.100 | 374. | 379. | -5. |
| 23.300 | 354. | 354. | 0.  |
| 23.500 | 340. | 331. | 9.  |
| 23.700 | 328. | 312. | 16. |
| 23.900 | 316. | 294. | 22. |
| 24.100 | 304. | 279. | 25. |
| 24.300 | 300. | 265. | 35. |
| 24.500 | 290. | 251. | 39. |
| 24.700 | 268. | 237. | 31. |
| 24.900 | 252. | 223. | 29. |
| 25.100 | 228. | 211. | 17. |
| 25.300 | 212. | 200. | 12. |
| 25.500 | 210. | 190. | 20. |
| 25.700 | 200. | 181. | 19. |
| 25.900 | 200. | 172. | 28. |
| 26.100 | 194. | 164. | 30. |
| 26.300 | 190. | 156. | 34. |
| 26.500 | 190. | 148. | 42. |
| 26.700 | 180. | 141. | 39. |
| 26.900 | 176. | 135. | 41. |
| 27.100 | 170. | 129. | 41. |
| 27.300 | 162. | 123. | 39. |
| 27.500 | 160. | 118. | 42. |
| 27.700 | 158. | 112. | 46. |
| 27.900 | 150. | 107. | 43. |
| 28.100 | 150. | 103. | 47. |
| 28.300 | 150. | 98.  | 52. |
| 28.500 | 150. | 94.  | 56. |
| 28.700 | 148. | 89.  | 59. |
| 28.900 | 140. | 85.  | 55. |
| 29.100 | 140. | 81.  | 59. |
| 29.300 | 140. | 78.  | 62. |
| 29.500 | 140. | 75.  | 65. |
| 29.700 | 140. | 72.  | 68. |
| 29.900 | 136. | 69.  | 67. |
| 30.100 | 124. | 67.  | 57. |
| 30.300 | 120. | 64.  | 56. |
| 30.500 | 120. | 61.  | 59. |
| 30.700 | 120. | 59.  | 61. |
| 30.900 | 120. | 56.  | 64. |
| 31.100 | 114. | 54.  | 60. |
| 31.300 | 110. | 52.  | 58. |
| 31.500 | 110. | 49.  | 61. |
| 31.700 | 110. | 47.  | 63. |
| 31.900 | 110. | 45.  | 65. |
| 32.100 | 110. | 42.  | 68. |
| 32.300 | 102. | 40.  | 62. |
| 32.500 | 100. | 38.  | 62. |

ERROR STANDARD DEVIATION = 177.294  
 PEAK DISCHARGE ERROR = 3.99 PERCENT

\* THIS COMPLETES THE ROUTING FOR THE WATERSHED IN ITS PRESENT CONDITION. \*  
 \* NEXT ASSUME FLOOD DETENTION RESERVOIRS ARE CONSTRUCTED TO CONTROL THE RUNOFF \*  
 \* FROM AREAS 301 AND 306. TO EVALUATE THE EFFECTS OF THESE RESERVOIRS ON THE \*  
 \* FLOOD HYDROGRAPH THE FLOOD OF MARCH 29, 1965 IS ROUTED THROUGH THE WATERSHED \*  
 \* WITH THE RESERVOIRS INSTALLED. SINCE THE PUNCH CODE WAS USED FOR THE FIRST \*  
 \* ROUTING, ALL CARDS FOR THE SECOND ROUTING WERE PUNCHED BY THE COMPUTER. \*  
 \* HOWEVER, ROUTE RESERVOIR COMMANDS MUST BE MANUALLY PUNCHED AND PLACED IN THE \*  
 \* PROGRAM TO ROUTE THROUGH THE PROPOSED RESERVOIRS. ALSO SOME OF THE COMPUTER \*  
 \* PUNCHED COMMENT CARDS ARE CHANGED OR DELETED. \*  
 \* THE FIRST STEP IS TO STORE THE HYD FROM AREA 301. NOTICE THE ID NUMBER IS \*  
 \* CHANGED FROM 1 TO 5 SO THE RESERVOIR OUTFLOW CAN BE STORED IN ID 1 TO MAKE IT \*  
 \* COMPATIBLE WITH THE STORE TRAVEL TIME AND ROUTE COMMANDS FOR REACH 2. \*  
 \*  
 \* RECALL HYD      ID=5    HYD NO=301    DT= 0.166667 HRS    DA= 1.734 SQ MI  
                  PEAK= 2360.CFS    RD= 4.933 INCHES    NO PTS=105    FLOW RATE  
                  0.            0.            0.            0.            0.            20.  
                  90.           220.           1025.           1420.           1380.           2085.           2260.  
                  2360.           2110.           1885.           1890.           1760.           1560.           1350.  
                  1150.           1000.           860.           690.           560.           460.           400.  
                  370.           365.           380.           400.           415.           395.           370.  
                  330.           300.           270.           235.           200.           175.           160.  
                  140.           130.           120.           110.           110.           110.           110.  
                  110.           100.           100.           90.           80.           70.           65.  
                  60.           50.           47.           44.           41.           38.           35.  
                  33.           31.           29.           27.           25.           23.           22.  
                  20.           18.           17.           16.           15.           14.           13.  
                  12.           11.           10.           10.           9.           9.           8.  
                  8.           7.           7.           6.           6.           6.           5.  
                  5.           4.           4.           4.           4.           4.           3.  
                  3.           3.           3.           2.           2.           2.           1.

| ROUTE | RESERVOIR | ID=1   | HVD NO=501     | INFLOW | ID=5 | REMAINING |
|-------|-----------|--|----------------|--------|------|-----------|
|       |           | DATA DEFINE RESERVOIR OUTFLOW STORAGE RELATIONSHIP |                |        |      |           |
|       |           | OUTFLW(CFS)  | STORAGE(AC FT) |        |      |           |
|       |           | 0  | 50             |        |      |           |
|       |           | 22   | 533            |        |      |           |
|       |           | 200  | 555            |        |      |           |
|       |           | 1000   | 601            |        |      |           |
|       |           | 2000   | 648            |        |      |           |
|       |           | 3000   | 694            |        |      |           |

```

**
PRINT HYD
ID=1

```

## OUTFLOW HYDROGRAPH RESERVOIR 501

[illegible]

RUNOFF VOLUME = 0.382 INCHES  
PEAK DISCHARGE RATE = 20.0 CFS

\* NEXT ROUTE THE OUTFLOW HYD FROM RESERVOIR 501 THROUGH REACH 2.  
 \* BEFORE ROUTING THE TRAVEL TIME - DEPTH - FLOW RELATIONSHIP MUST BE COMPUTED  
 \* FOR THE REACH.

| STORE TRAVEL TIME | ID=2      | REACH NO=           | 2.0         | LENGTH= | 3400. FT |                |
|-------------------|-----------|---------------------|-------------|---------|----------|----------------|
|                   |           | SLOPE=0.002900FT/FT |             |         |          |                |
|                   | DEPTH(FT) | FLOW(CFS)           | TIME(HRS)   |         |          |                |
|                   | 0.30      | 2.                  | 0.832       |         |          |                |
|                   | 0.68      | 6.                  | 0.597       |         |          |                |
|                   | 1.07      | 16.                 | 0.498       |         |          |                |
|                   | 1.58      | 38.                 | 0.472       |         |          |                |
|                   | 2.18      | 86.                 | 0.390       |         |          |                |
|                   | 2.75      | 153.                | 0.338       |         |          |                |
|                   | 3.28      | 252.                | 0.343       |         |          |                |
|                   | 3.66      | 371.                | 0.364       |         |          |                |
|                   | 4.02      | 545.                | 0.359       |         |          |                |
|                   | 4.45      | 910.                | 0.359       |         |          |                |
|                   | 4.78      | 1064.               | 0.350       |         |          |                |
|                   | 5.13      | 1431.               | 0.363       |         |          |                |
|                   | 5.50      | 1980.               | 0.353       |         |          |                |
|                   | 5.86      | 2672.               | 0.341       |         |          |                |
|                   | 6.29      | 3670.               | 0.336       |         |          |                |
|                   | 6.67      | 4853.               | 0.332       |         |          |                |
|                   | 6.98      | 6225.               | 0.307       |         |          |                |
|                   | 7.29      | 7793.               | 0.286       |         |          |                |
|                   | 7.60      | 9613.               | 0.267       |         |          |                |
| ROUTE             | ID=2      | HYD NO=101          | INFLOW ID=1 |         |          | DT=0.200000HRS |
| PRINT HYD         | ID=2      | CODE=1              |             |         |          |                |

PARTIAL HYDROGRAPH 101

RUNOFF VOLUME = 0.411 INCHES  
 PEAK DISCHARGE RATE = 20.0 CFS

TO OBTAIN THE OUTFLOW HYD FROM REACH 2 THE HYD FROM AREA 302 MUST BE COMPUTED\*  
 ANC ADDED TO THE ROUTED HYD 101.

RECALL HYD ID=1 HYD NO=302 DT= 0.166667 HRS DA= 0.837 SQ MI  
 PEAK= 572.CFS RO= 4.124 INCHES NO PTS=154  
 FLOW RATES

|      |      |      |      |      |      |
|------|------|------|------|------|------|
| 0.   | 0.   | 0.   | 1.   | 2.   | 9.   |
| 36.  | 89.  | 169. | 332. | 411. | 491. |
| 548. | 570. | 572. | 532. | 495. | 451. |
| 407. | 363. | 328. | 282. | 264. | 244. |
| 223. | 204. | 193. | 211. | 219. | 219. |
| 212. | 201. | 188. | 160. | 147. | 135. |
| 125. | 115. | 109. | 124. | 127. | 128. |
| 125. | 120. | 113. | 99.  | 92.  | 86.  |
| 81.  | 75.  | 70.  | 61.  | 57.  | 53.  |
| 49.  | 46.  | 43.  | 37.  | 35.  | 33.  |
| 32.  | 30.  | 29.  | 26.  | 25.  | 24.  |
| 23.  | 22.  | 21.  | 19.  | 19.  | 18.  |
| 17.  | 16.  | 16.  | 14.  | 14.  | 13.  |
| 13.  | 12.  | 12.  | 11.  | 10.  | 10.  |
| 9.   | 9.   | 9.   | 8.   | 8.   | 7.   |
| 7.   | 6.   | 6.   | 5.   | 4.   | 4.   |
| 3.   | 3.   | 3.   | 2.   | 2.   | 2.   |
| 2.   | 2.   | 2.   | 1.   | 1.   | 1.   |
| 1.   | 1.   | 1.   | 1.   | 1.   | 1.   |
| 0.   | 0.   | 0.   | 0.   | 0.   | 0.   |
| 0.   | 0.   | 0.   | 0.   | 0.   | 0.   |
| 0.   | 0.   | 0.   | 0.   | 0.   | 0.   |

✱

IO I I = 2

$$I=1$$

HYD NO= 2  
CODE=0

ID=3  
ID=3

ADD HYD  
PRINT HYD

OUTFLOW HYDROGRAPH REACH 2

[illegible]

\* ROUTE THROUGH REACH 3.  
\*

| STORE TRAVEL TIME | ID=1      | REACH NO=           | 3.0    | LENGTH= | 3330. FT       |
|-------------------|-----------|---------------------|--------|---------|----------------|
|                   |           | SLOPE=0.002450FT/FT |        |         |                |
| DEPTH(FT)         | FLOW(CFS) | TIME(HRS)           |        |         |                |
| 0.45              | 2.        | 0.862               |        |         |                |
| 0.96              | 10.       | 0.548               |        |         |                |
| 1.45              | 23.       | 0.414               |        |         |                |
| 1.92              | 41.       | 0.343               |        |         |                |
| 2.37              | 63.       | 0.299               |        |         |                |
| 2.80              | 90.       | 0.267               |        |         |                |
| 3.22              | 122.      | 0.245               |        |         |                |
| 3.58              | 160.      | 0.253               |        |         |                |
| 3.99              | 215.      | 0.270               |        |         |                |
| 4.32              | 287.      | 0.291               |        |         |                |
| 4.69              | 403.      | 0.316               |        |         |                |
| 5.10              | 592.      | 0.324               |        |         |                |
| 5.57              | 887.      | 0.327               |        |         |                |
| 6.03              | 1273.     | 0.321               |        |         |                |
| 6.45              | 1724.     | 0.337               |        |         |                |
| 6.91              | 2527.     | 0.335               |        |         |                |
| 7.40              | 3561.     | 0.333               |        |         |                |
| 7.86              | 4956.     | 0.329               |        |         |                |
| 8.31              | 6826.     | 0.304               |        |         |                |
| ROUTE             | ID=1      | HYD NO=102          | INFLOW | ID=3    | DT=0.200000HRS |
| PRINT HYD         | ID=1      | CODE=1              |        |         |                |

PARTIAL HYDROGRAPH 102

RUNOFF VOLUME = 1.619 INCHES  
PEAK DISCHARGE RATE = 536.6 CFS

```

* COMPUTE THE HYD FROM AREA 303.
*
RECALL HYD      ID=2  HYD NO=303  DT= 0.166667 HRS  DA= 1.108 SQ MI
PEAK= 674.CFS  RO= 4.131 INCHES  NO PTS=175
FLOW RATES
0.      0.      0.      0.      1.      2.      8.
33.     84.     164.    253.    341.    433.    528.
604.    671.    674.    660.    660.    632.    594.
550.    504.    462.    428.    404.    379.    354.
328.    304.    287.    281.    292.    297.    295.
285.    273.    257.    240.    223.    206.    191.
177.    164.    155.    160.    165.    168.    169.
166.    162.    155.    148.    140.    132.    125.
118.    110.    103.    97.     90.     85.     80.
75.     71.     67.     63.     60.     56.     53.
51.     48.     46.     43.     42.     40.     38.
37.     35.     34.     33.     32.     31.     29.
28.     27.     26.     26.     25.     24.     23.
22.     21.     21.     20.     19.     19.     18.
17.     17.     16.     16.     15.     14.     14.
15.     13.     13.     12.     12.     11.     11.
11.     10.     10.     9.      9.      9.      8.
8.      8.      8.      7.      7.      7.      7.
6.      6.      5.      5.      4.      4.      3.
3.      2.      2.      2.      2.      2.      2.
2.      2.      2.      1.      1.      1.      1.
1.      1.      1.      1.      1.      0.      0.
0.      0.      0.      0.      0.      0.      0.
0.      0.      0.      0.      0.      0.      0.
0.      0.      0.      0.      0.      0.      0.

```





\* ROUTE THROUGH REACH 4.

\* STORE TRAVEL TIME ID=1 REACH NO= 4.0 LENGTH= 3415. FT  
SLOPE=0.003000FT/FT  
DEPTH(FT) FLOW(CFS) TIME(HRS)  
0.38 2. 0.878  
0.84 7. 0.614  
1.25 15. 0.472  
1.69 28. 0.390  
2.14 45. 0.339  
2.54 62. 0.319  
3.15 104. 0.268  
3.75 155. 0.233  
4.32 223. 0.208  
4.87 305. 0.200  
5.36 403. 0.202  
5.82 554. 0.231  
6.32 814. 0.251  
6.83 1196. 0.249  
7.28 1598. 0.253  
7.69 2078. 0.262  
8.27 3122. 0.257  
8.86 4498. 0.246  
9.47 6405. 0.230  
ROUTE ID=1 HYD NO=103 INFLOW ID=3  
PRINT HYD ID=1 CODE=1 DT=0.200000HRS

PARTIAL HYDROGRAPH 103

RUNOFF VOLUME = 2.375 INCHES  
PEAK DISCHARGE RATE = 1159.1 CFS

\* COMPUTE THE HYD FROM AREA 304.

\* RECALL HYD ID=2 HYD NO=304 DT= 0.250000 HRS DA= 0.807 SQ MI  
PEAK= 504.CFS RQ= 4.111 INCHES NO PTS=119  
FLOW RATES  
0. 0. 0. 1. 8. 53. 153.  
259. 359. 457. 499. 504. 482. 438.  
385. 336. 299. 275. 248. 220. 201.  
211. 218. 217. 207. 192. 173.  
154. 137. 122. 108. 97. 88. 79.  
72. 66. 60. 54. 51. 51. 49.  
47. 43. 41. 39. 37. 35.  
33. 30. 28. 24. 23. 21.  
20. 19. 18. 17. 16. 15. 14.  
13. 12. 11. 11. 10. 9.  
9. 8. 8. 8. 7. 6.  
6. 5. 4. 4. 3. 2. 2.  
2. 2. 2. 2. 1. 1. 1.  
1. 1. 1. 1. 0. 0. 0.  
0. 0. 0. 0. 0. 0. 0.  
0. 0. 0. 0. 0. 0. 0.

\* ADD THE H  
\* REACH 4.

```

ID=3      ADD HYD      ID I=1      ID I=2
ID=3      PRINT HYD    CODE=0

```

## OUTFLOW HYDROGRAPH REACH 4

[illegible]

RUNOFF VOLUME = 2.686 INCHES

PEAK DISCHARGE RATE = 1630.0 CFS

```

* ROUTE THROUGH REACH 5.
*
STORE TRAVEL TIME ID=1 REACH NO= 5.0 LENGTH= 3310. FT
SLOPE=0.003000FT/FT
DEPTH(FT) FLOW(CFS) TIME(HRS)
0.35 2. 0.749
0.96 9. 0.542
1.57 26. 0.400
2.19 52. 0.317
2.82 90. 0.267
3.45 141. 0.231
4.28 237. 0.220
5.30 461. 0.210
6.13 818. 0.208
6.83 1317. 0.195
7.47 1958. 0.177
8.09 2750. 0.161
8.71 3713. 0.148
9.31 4861. 0.137
9.78 5889. 0.132
10.18 6694. 0.132
10.77 8589. 0.127
11.33 11067. 0.120
11.89 14199. 0.113
ROUTE ID=1 HYD NO=104 INFLOW ID=3 DT=0.200005HRS
PRINT HYD ID=1 CODE=1

```

PARTIAL HYDROGRAPH 104

```

RUNOFF VOLUME = 2.686 INCHES
PEAK DISCHARGE RATE = 1610.2 CFS

```

```

RECALL HYD ID=2 HYD NO=305 DT= 0.333333 HRS DA= 1.875 SQ MI
PEAK= 937.CFS RO= 3.837 INCHES NO PTS=117
FLOW RATES
0. 0. 2. 28. 157. 363.
614. 821. 924. 937. 880. 793. 729.
674. 610. 550. 517. 474. 425. 373.
324. 278. 240. 216. 197. 182. 167.
155. 145. 136. 128. 119. 111. 104.
98. 93. 87. 81. 75. 70. 65.
60. 56. 52. 49. 46. 43. 41.
38. 36. 34. 32. 30. 29. 27.
26. 24. 23. 22. 21. 20. 18.
17. 17. 16. 15. 14. 13. 12.
12. 11. 11. 10. 9. 8. 6.
8. 7. 7. 6. 6. 6. 6.
5. 5. 4. 3. 2. 1. 1.
1. 1. 1. 1. 1. 1. 1.
0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0.

```

ADD THE HYD FROM AREA 305 TO THE PARTIAL HYD 104.

ADD HYD ID=3 HYD NO=105 ID I=1 ID II=2  
PRINT HYD ID=3 CODE=1

PARTIAL HYDROGRAPH 105

RUNOFF VOLUME = 3.025 INCHES  
PEAK DISCHARGE RATE = 2542.0 CFS

\* THE HYD FROM AREA 306 IS RECALLED AND USED AS THE INFLOW HYD TO RESERVOIR 502

\* RECALL HYD ID=5 HYD NO=306 DT= 0.250000 HRS DA= 0.483 SO MI  
PEAK= 698.CFS RD= 3.369 INCHES NO PTS= 61 FLOW RATE  
0. 0. 0. 45. 280. 560.  
638. 570. 370. 258. 170. 97. 72.  
64. 61. 80. 70. 59. 54. 52.  
51. 50. 46. 44. 40. 38. 33.  
30. 27. 25. 24. 23. 22. 21.  
20. 20. 19. 18. 16. 15. 15.  
13. 11. 10. 9. 8. 7. 6.  
5. 5. 4. 4. 3. 3. 3.  
3. 2. 2. 1. 1.

\* ROUTE THE HYD FROM AREA 306 THROUGH RESERVOIR 502.

\* ROUTE RESERVOIR ID=1 HYD NO=502 INFLOW ID=5  
OUTFLOW(CFS) STORAGE(AC FT)  
0 1 2 5  
0 .1 2.5  
.2 5  
.4 8  
.6 15  
6. 148  
50 155  
200 167  
500 180  
PRINT HYD ID=1 CODE=1

OUTFLOW HYDROGRAPH RESERVOIR 502

RUNOFF VOLUME = 0.369 INCHES  
PEAK DISCHARGE RATE = 3.4 CFS

```

* ROUTE OUTFLOW FROM RESERVOIR 502 THROUGH REACH 6.
*
STORE TRAVEL TIME ID=2 REACH NO= 6.0 LENGTH= 4080. FT
SLOPE=0.007500FT/FT
DEPTH(FT) FLOW(CFS) TIME(HRS)
0.44 5. 0.589
0.80 16. 0.406
1.18 33. 0.335
1.52 56. 0.285
1.88 88. 0.252
2.26 146. 0.249
2.66 251. 0.248
3.10 421. 0.240
3.55 675. 0.228
4.00 1019. 0.216
4.46 1482. 0.205
4.93 2102. 0.192
5.40 2902. 0.179
5.88 3908. 0.167
6.37 5214. 0.154
6.85 6796. 0.142
7.33 8649. 0.132
7.80 10796. 0.123
8.28 13261. 0.116
ROUTE ID=2 HYD NO=106 INFLOW ID=1
PRINT HYD ID=2 CODE=1
DT=0.200000HRS
PARTIAL HYDROGRAPH 106

RUNOFF VOLUME = 0.381 INCHES
PEAK DISCHARGE RATE = 3.4 CFS

```



\* THE SEDIMENT YIELD COMMAND IS USED TO COMPUTE THE SEDIMENT YIELD PRODUCED BY \*  
 \* THE ROUTED FLOOD.

\* SEDIMENT YIELD ID=6 SCIL=.34 CROP=.16 CP=.4 LS=.3  
 SEDIMENT YIELD = 2444.6 TONS

\* RECALL THE REACH 5 OUTFLOW HYD ROUTED WITH PRESENT CONDITIONS.

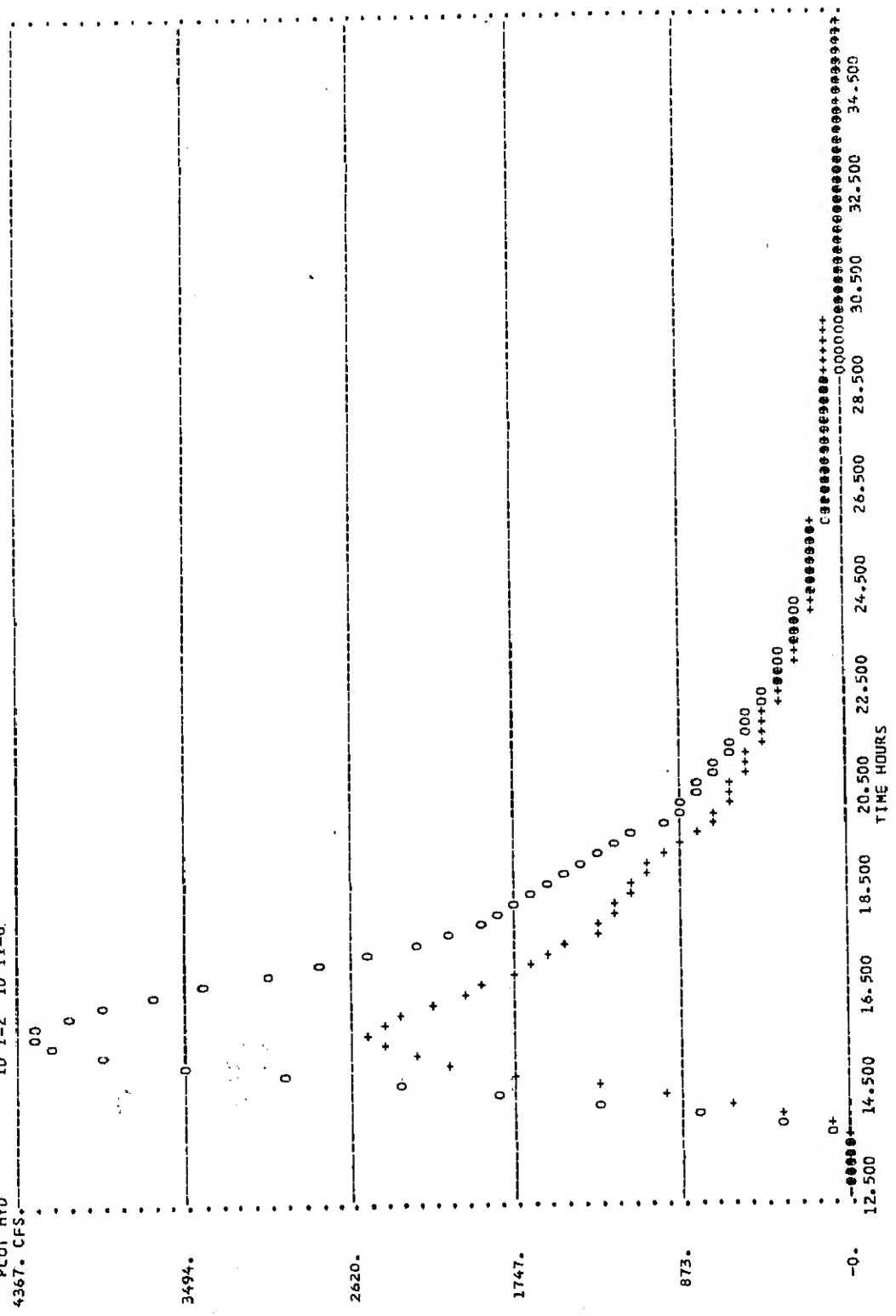
\* RECALL HYD

ID=2 HYD NO= 5 DT= 0.200000 HRS DA= 6.844 SQ MI  
 PEAK= 4367.CFS RO= 4.196 INCHES NO PTS=194

| FLOW RATES | 0.    | 0.    | 0.    | 0.    | 3.    | 15.   | 106. |
|------------|-------|-------|-------|-------|-------|-------|------|
| 378.       | 829.  | 1349. | 1855. | 2403. | 2983. | 3537. |      |
| 3968.      | 4260. | 4367. | 4337. | 4181. | 3950. | 3684. |      |
| 3415.      | 3143. | 2880. | 2611. | 2353. | 2137. | 1978. |      |
| 1869.      | 1783. | 1707. | 1628. | 1541. | 1446. | 1347. |      |
| 1244.      | 1141. | 1044. | 959.  | 889.  | 833.  | 788.  |      |
| 749.       | 714.  | 678.  | 641.  | 604.  | 568.  | 532.  |      |
| 497.       | 466.  | 436.  | 407.  | 379.  | 354.  | 331.  |      |
| 312.       | 294.  | 279.  | 265.  | 251.  | 237.  | 223.  |      |
| 211.       | 200.  | 190.  | 181.  | 172.  | 164.  | 156.  |      |
| 148.       | 141.  | 135.  | 129.  | 123.  | 118.  | 112.  |      |
| 107.       | 103.  | 98.   | 94.   | 89.   | 85.   | 81.   |      |
| 78.        | 75.   | 72.   | 69.   | 67.   | 64.   | 61.   |      |
| 59.        | 56.   | 54.   | 52.   | 49.   | 47.   | 45.   |      |
| 42.        | 40.   | 38.   | 36.   | 35.   | 33.   | 31.   |      |
| 30.        | 29.   | 28.   | 26.   | 25.   | 24.   | 22.   |      |
| 21.        | 20.   | 19.   | 18.   | 17.   | 16.   | 15.   |      |
| 15.        | 14.   | 13.   | 13.   | 12.   | 12.   | 11.   |      |
| 11.        | 10.   | 10.   | 9.    | 9.    | 7.    | 7.    |      |
| 7.         | 7.    | 6.    | 6.    | 6.    | 6.    | 6.    |      |
| 5.         | 5.    | 5.    | 5.    | 4.    | 4.    | 3.    |      |
| 3.         | 3.    | 2.    | 1.    | 1.    | 1.    | 1.    |      |
| 1.         | 1.    | 1.    | 1.    | 1.    | 1.    | 1.    |      |
| 1.         | 1.    | 0.    | 0.    | 0.    | 0.    | 0.    |      |
| 0.         | 0.    | 0.    | 0.    | 0.    | 0.    | 0.    |      |
| 0.         | 0.    | 0.    | 0.    | 0.    | 0.    | 0.    |      |
| 0.         | 0.    | 0.    | 0.    | 0.    | 0.    | 0.    |      |
| 0.         | 0.    | 0.    | 0.    | 0.    | 0.    | 0.    |      |



\* PLOT THE REACH 5 OUTFLOW HYDS ROUTED WITH PRESENT CONDITIONS AND WITH \*  
 \* RESERVOIRS.  
 \* PLOT SYMBOLS PRESENT CONDITIONS--O-- WITH RESERVOIRS--+-  
 PLOT HYD ID 1-2 ID 11-6.  
 4367. CFS.



FINISH

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## APPENDIX

### HYMO MAIN PROGRAM AND SUBROUTINES

54

|    |    |   |   |     |
|----|----|---|---|-----|
| 35 |    | GO TO 1   | A | 60  |
| 36 | 13 | CALL STT  | A | 61  |
| 37 |    | GO TO 1   | A | 62  |
| 38 | 14 | CALL CMPTT  | A | 63  |
| 39 |    | GO TO 1   | A | 64  |
| 40 | 15 | CALL ROUTE  | A | 65  |
| 41 |    | GO TO 1   | A | 66  |
| 42 | 16 | CALL RESVO  | A | 67  |
| 43 |    | GO TO 1   | A | 68  |
| 44 | 17 | CALL ERROR  | A | 69  |
| 45 |    | GO TO 1   | A | 70  |
| 46 | 18 | CALL SEDT   | A | 71  |
| 47 |    | GO TO 1   | A | 72  |
| 48 | 19 | STOP  | A | 73  |
|    | C  |   | A | 74  |
| 49 | 20 | FORMAT (15A1)   | A | 75  |
| 50 | 21 | FORMAT (I2)   | A | 76  |
| 51 | 22 | FORMAT (2A1,9A2,2I3)  | A | 77  |
| 52 | 23 | FORMAT (1H1,9X,8HZALFA = ,15A1///)                                  | A | 78  |
| 53 | 24 | FORMAT (16X,13HCOMMAND TABLE//)                                     | A | 79  |
| 54 | 25 | FORMAT (10X,2A1,9A2,2I3)  | A | 80  |
| 55 |    | END   | A | 81- |
| 56 |    | SUBROUTINE HONDO  | B | 1   |
|    | C  | THIS SUBROUTINE READS IN A DATA CARD , SEARCHES AN ALPHAMERIC       | B | 2   |
|    | C  | CODE TABLE TO DETERMINE THE NCODE OF THE OPERATION AND              | B | 3   |
|    | C  | COLLECTS VARIABLES FROM THE FREEFLOATING DATA FIELD                 | B | 4   |
| 57 |    | COMMON CFS(300),OCFS(300,6),IEND(6),DATA(310),DA(6),DP(20),NPU,NHD  | B | 5   |
|    |    | 1,SCFS(20),C(20),A(20,6),Q(20,6),RAIN(200),DEEP(20,6),NER,MAXNO,NCO | B | 6   |
|    |    | 2MM,ICC,NCODE,DIST(6),SEGN(6),CTBLE(50,11),ITBLE(50,2),ZALFA(20),DT | B | 7   |
|    |    | 3(6),TIME,PEAK(6),ROIN,ISG(6)                                       | B | 8   |
| 58 |    | DIMENSION CHAR(60), ALPHA(11)                                       | B | 9   |
| 59 |    | DIMENSION AUXA(10), AUXB(10)  | B | 10  |
| 60 |    | IF (ICC) 1,1,3  | B | 11  |
|    | C  | READ IN DATA CARD   | B | 12  |
| 61 | 1  | READ (5,42) (ALPHA(I),I=1,11),(CHAR(I),I=1,60)                      | B | 13  |
|    | C  | IF FIRST CHARACTER IS BLANK THE CARD IS A CONTINUATION OF           | B | 14  |
|    | C  | PREVIOUS CARD.  | B | 15  |
| 62 |    | IF (ALPHA(1)-ZALFA(11)) 2,9,2                                       | B | 16  |
| 63 | 2  | IF (ICC) 3,3,40   | B | 17  |
|    | C  | ASTERISK IN COL. 80 MEANS SKIP TO NEW PAGE BEFORE PRINTING CARD     | B | 18  |
| 64 | 3  | IF (CHAR(60)-ZALFA(11)) 4,5,4                                       | B | 19  |
| 65 | 4  | WRITE (6,43)  | B | 20  |
| 66 | 5  | WRITE (6,44) (ALPHA(I),I=1,11),(CHAR(I),I=1,60)                     | B | 21  |
|    | C  | IF FIRST CHARACTER IS A * THE PREVIOUS CARD WAS A COMMENT CARD      | B | 22  |
| 67 |    | IF (ALPHA(1)-ZALFA(12)) 10,6,10                                     | B | 23  |
|    | C  | IF PUNCH CODE POSITIVE, COMMENT CARDS ARE PUNCHED.                  | B | 24  |
| 68 | 6  | IF (NPU) 8,8,7  | B | 25  |
| 69 | 7  | WRITE (7,45) (ALPHA(I),I=1,11),(CHAR(I),I=1,60)                     | B | 26  |
| 70 | 8  | ICC=0   | B | 27  |
| 71 |    | GO TO 1   | B | 28  |
| 72 | 9  | WRITE (6,44) (ALPHA(I),I=1,11),(CHAR(I),I=1,60)                     | B | 29  |
| 73 |    | GO TO 24  | B | 30  |
|    | C  | SEARCH FIRST TWO ALPHAMERIC CHARACTERS TO SEE IF THEY ARE NUMBERS   | B | 31  |
| 74 | 10 | ICC=1   | B | 32  |
| 75 |    | DO 12 I=1,10  | B | 33  |
| 76 |    | IF (ALPHA(1)-ZALFA(I)) 11,15,11                                     | B | 34  |
| 77 | 11 | IF (ALPHA(2)-ZALFA(I)) 12,15,12                                     | B | 35  |
| 78 | 12 | CONTINUE  | B | 36  |
|    | C  | STATEMENT NUMBER 7 IS BRANCHED TO IF NUMBERS ARE PRESENT            | B | 37  |

|     |    |  |   |    |
|-----|----|--|---|----|
|     | C  | IF NOT NUMBER SEARCH COMMAND TABLE FOR MATCH                 | B | 38 |
|     | C  | CALL FIRST 10 VALUES FROM PERMANENT DATA STORAGE             | B | 39 |
| 79  |    | DO 14 I=1,50   | B | 40 |
| 80  |    | DO 13 J=1,11   | B | 41 |
| 81  |    | IF (CTBLE(I,J)-ALPHA(J)) 14,13,14                            | B | 42 |
|     | C  | SN 10=PART MATCH   | B | 43 |
| 82  | 13 | CONTINUE   | B | 44 |
|     | C  | IF THIS LOOP IS COMPLETED WE HAVE COMPLETE MATCH- CALL NCODE | B | 45 |
|     | C  | AND MAX NUMBER AND EXIT LOOP                                 | B | 46 |
| 83  |    | NCODE=ITBLE(1,1)   | B | 47 |
| 84  |    | MAXNO=ITBLE(1,2)   | B | 48 |
| 85  |    | GO TO 21   | B | 49 |
| 86  | 14 | CONTINUE   | B | 50 |
|     | C  | IF MAJOR LOOPS FINISHED WITHOUT A MATCH WRITE ERROR MESSAGE  | B | 51 |
|     | C  | AND SET NER = 1  | B | 52 |
| 87  |    | NER=1  | B | 53 |
| 88  |    | WRITE (6,46)   | B | 54 |
| 89  |    | RETURN   | B | 55 |
|     | C  | CONVERT DIGIT INPUT CODE FROM ALPHAMERIC TO INTEGER FORM     | B | 56 |
| 90  | 15 | NCODE=GIT(ALPHA,1,2,1.)*0.5                                  | B | 57 |
|     | C  | FIND MAX NUMBER OF DATA ITEMS FOR THIS NCODE                 | B | 58 |
| 91  |    | DO 17 I=1,50   | B | 59 |
| 92  |    | IF (ITBLE(1,1)-NCODE) 17,16,17                               | B | 60 |
| 93  | 16 | MAXNO=ITBLE(1,2)   | B | 61 |
| 94  |    | GO TO 21   | B | 62 |
| 95  | 17 | CONTINUE   | B | 63 |
|     | C  | SEARCH DATA ROUTINE  | B | 64 |
|     | C  | SEE IF ANY DATA FOR THIS CARD                                | B | 65 |
| 96  |    | DO 19 I=1,50   | B | 66 |
| 97  |    | IF (ITBLE(1,1)-NCODE) 19,18,19                               | B | 67 |
| 98  | 18 | MAXNO=ITBLE(1,2)   | B | 68 |
| 99  |    | GO TO 20   | B | 69 |
| 100 | 19 | CONTINUE   | B | 70 |
| 101 | 20 | CONTINUE   | B | 71 |
| 102 | 21 | IF (MAXNO) 23,22,23  | B | 72 |
| 103 | 22 | RETURN   | B | 73 |
|     | C  | ZERO ARRAYS AND COUNTERS                                     | B | 74 |
| 104 | 23 | DO 47 I=1,310  | B | 75 |
| 105 | 47 | DATA (I)=0.  | B | 76 |
| 106 |    | NDATA=1  | B | 77 |
| 107 | 24 | NCHAR=0  | B | 78 |
| 108 | 25 | DO 26 I=1,10   | B | 79 |
| 109 |    | AUXA(I)=0.   | B | 80 |
| 110 | 26 | AUXB(I)=0.   | B | 81 |
| 111 |    | IT1=1  | B | 82 |
| 112 |    | IT2=1  | B | 83 |
| 113 |    | SIGN=1.  | B | 84 |
| 114 |    | LDGIT=0  | B | 85 |
| 115 |    | KDGIT=0  | B | 86 |
|     | C  | CARRY OUT DIGIT BY DIGIT SEARCH AND ACCUMULATION             | B | 87 |
| 116 | 27 | NCHAR=NCHAR+1  | B | 88 |
|     | C  | HAVE WE CONSIDERED ALL CHARACTERS - RETURN IF SO             | B | 89 |
| 117 |    | IF (NCHAR-60) 28,32,1  | B | 90 |
| 118 | 28 | DO 29 I=1,15   | B | 91 |
| 119 |    | IF (CHAR(NCHAR)-ZALFA(I)) 29,30,29                           | B | 92 |
| 120 | 29 | CONTINUE   | B | 93 |
| 121 |    | GO TO 32   | B | 94 |
| 122 | 30 | GO TO (33,33,33,33,33,33,33,33,33,33,32,27,36,32,31,27), I   | B | 95 |
|     | C  | SN 39 HANDLES SIGN CONTROL ON 1130 VERSION                   | B | 96 |
| 123 | 31 | SIGN=-1.0  | B | 97 |

|     |    |  |        |
|-----|----|--|--------|
| 124 |    | GO TO 27   | B 98   |
|     | C  | CHARACTER IS BLANK OR COMMA - DOES IT FOLLOW A DIGIT             | B 99   |
| 125 | 32 | GO TO (27,48), IT1   | B 100  |
|     | C  | CHARACTER IS A DIGIT - HAS A DECIMAL BEEN ENCOUNTERED            | B 101  |
| 126 | 33 | GO TO (34,35), IT2   | B 102  |
| 127 | 34 | LDGIT=LDGIT+1  | B 103  |
| 128 |    | IT1=2  | B 104  |
| 129 |    | AUXA(LDGIT)=CHAR(NCHAR)  | B 105  |
| 130 |    | GO TO 27   | B 106  |
| 131 | 35 | KDGIT=KDGIT+1  | B 107  |
| 132 |    | AUXB(KDGIT)=CHAR(NCHAR)  | B 108  |
| 133 |    | GO TO 27   | B 109  |
|     | C  | CHARACTER IS A DECIMAL - DOES IT FOLLOW A DIGIT                  | B 110  |
| 134 | 36 | GO TO (37,38), IT1   | B 111  |
| 135 | 37 | IT1=2  | B 112  |
| 136 |    | LDGIT=1  | B 113  |
| 137 | 38 | IT2=2  | B 114  |
| 138 |    | GO TO 27   | B 115  |
|     | C  | ROUTINE TO CONVERT ALPHABETIC ARRAY TO FLOATING POINT NUMBER     | B 116  |
| 139 | 48 | DATA (NDATA)=GIT(AUXA,1,LDGIT,1.)*GIT(AUXB,1,10,0.)              | B 117  |
| 140 |    | DATA (NDATA)=DATA(NDATA)*SIGN                                    | B 118  |
|     | C  | IS ALL DATA FURNISHED YES-RETURN NO INCREASE N DATA KEEP ON      | B 119  |
| 141 |    | IF (NDATA-MAXNO) 41,39,39  | B 120  |
| 142 | 39 | ICC=0  | B 121  |
| 143 | 40 | RETURN   | B 122  |
| 144 | 41 | NDATA=NDATA+1  | B 123  |
| 145 |    | GO TO 25   | B 124  |
|     | C  |  | B 125  |
| 146 | 42 | FORMAT (2A1,9A2,60A1)  | B 126  |
| 147 | 43 | FORMAT (1H1)   | B 127  |
| 148 | 44 | FORMAT (5X,2A1,9A2,60A1)   | B 128  |
| 149 | 45 | FORMAT (2A1,9A2,60A1)  | B 129  |
| 150 | 46 | FORMAT (10X,20HCOMMAND NOT IN TABLE)                             | B 130  |
| 151 |    | END  | B 131- |
| 152 |    | FUNCTION GIT (TCARD,J,JLAST,SHIFT)                               | C 1    |
| 153 |    | DIMENSION TCARD(10), A(10)                                       | C 2    |
| 154 |    | DATA A(1)/1H1/,A(2)/1H2/,A(3)/1H3/,A(4)/1H4/,A(5)/1H5/,A(6)/1H6/ | C 3    |
| 155 |    | DATA A(7)/1H7/,A(8)/1H8/,A(9)/1H9/,A(10)/1H0/                    | C 4    |
| 156 |    | GIT=0.   | C 5    |
| 157 |    | TEN=10.  | C 6    |
| 158 |    | SUM=0.   | C 7    |
| 159 |    | DO 3 JNOW=J,JLAST  | C 8    |
| 160 |    | TTEST=TCARD(JNOW)  | C 9    |
|     | C  | CHECK FOR LAST ENTRY   | C 10   |
| 161 |    | IF (TTEST.EQ.0.) GO TO 4   | C 11   |
|     | C  | FIND NUMBER AND COMPUTE VALUE                                    | C 12   |
| 162 |    | DO 2 NUMB=1,10   | C 13   |
| 163 |    | IF (TTEST-A(NUMB)) 2,1,2   | C 14   |
| 164 | 1  | ZTEST=NUMB   | C 15   |
| 165 |    | IF (ZTEST.EQ.10.) ZTEST=0.                                       | C 16   |
| 166 |    | SUM=SUM*TEN+ZTEST  | C 17   |
| 167 |    | GO TO 3  | C 18   |
| 168 | 2  | CONTINUE   | C 19   |
| 169 | 3  | CONTINUE   | C 20   |
| 170 | 4  | IF (SHIFT) 6,5,6   | C 21   |
| 171 | 5  | FI=JNOW-1  | C 22   |
| 172 |    | SUM=SUM*(0.1**FI)  | C 23   |
| 173 | 6  | GIT=SUM  | C 24   |
| 174 |    | RETURN   | C 25   |

|     |   |   |     |
|-----|---|---|-----|
| 175 | END   | C | 26- |
| 176 | SUBROUTINE STHYD  | D | 1   |
| 177 | C THIS SUBROUTINE STORES THE COORDINATES OF HYDROGRAPHS.            | D | 2   |
|     | COMMON CFS(300),OCFS(300,6),IEND(6),DATA(310),DA(6),DP(20),NPU,NHD  | D | 3   |
|     | 1,SCFS(20),C(20),A(20,6),Q(20,6),RAIN(200),DEEP(20,6),NER,MAXNO,NCO | D | 4   |
|     | 2MM,ICC,NCODE,DIST(6),SEGN(6),CTBLE(50,11),ITBLE(50,2),ZALFA(20),DT | D | 5   |
|     | 3(6),TIME,PEAK(6),ROIN,ISG(6)                                       | D | 6   |
| 178 | ID=DATA(1)  | D | 7   |
| 179 | NHD=DATA(2)   | D | 8   |
| 180 | DT(ID)=DATA(3)  | D | 9   |
| 181 | DA(ID)=DATA(4)  | D | 10  |
| 182 | J=5   | D | 11  |
|     | C REMAINING DATA ARE FLOW RATES                                     | D | 12  |
| 183 | OCFS(1,ID)=DATA(J)  | D | 13  |
| 184 | PEAK(ID)=1.   | D | 14  |
| 185 | RO=DATA(J)  | D | 15  |
| 186 | DO 4 I=2,300  | D | 16  |
| 187 | J=J+1.  | D | 17  |
| 188 | OCFS(I,ID)=DATA(J)  | D | 18  |
| 189 | RO=RO+OCFS(I,ID)  | D | 19  |
|     | C IS FLOW RECEDING  | D | 20  |
| 190 | IF (OCFS(I,ID)-OCFS(I-1,ID)) 1,2,2                                  | D | 21  |
|     | C HAS FLOW RECEDED TO CUTOFF RATE                                   | D | 22  |
| 191 | IF (OCFS(I,ID)) 5,5,4   | D | 23  |
|     | C DETERMINE PEAK FLOW   | D | 24  |
| 192 | IF (OCFS(I,ID)-PEAK(ID)) 4,4,3                                      | D | 25  |
| 193 | PEAK(ID)=OCFS(I,ID)   | D | 26  |
| 194 | CONTINUE  | D | 27  |
| 195 | IEND(ID)=I-1  | D | 28  |
| 196 | M=IEND(ID)  | D | 29  |
| 197 | ROIN=(RO*DT(ID))/(DA(ID)*645.333)                                   | D | 30  |
|     | C PUNCH CODE  | D | 31  |
| 198 | IF (NPU) 7,7,6  | D | 32  |
| 199 | 6 WRITE (7,8) ID,NHD,DT(ID),DA(ID),PEAK(ID),ROIN,IEND(ID)           | D | 33  |
| 200 | WRITE (7,9) (OCFS(J,ID),J=1,M)                                      | D | 34  |
| 201 | 7 RETURN  | D | 35  |
|     | C   | D | 36  |
| 202 | 8 FORMAT( 'RECALL HYD',T21,'ID=',I1,T29,'HYD NO=',I3,T42,'DT=',F9.  | D | 37  |
|     | 16,' HRS',T61,'DA=',F8.3,' SQ MI'/T21,'PEAK=',F7.0,'CFS',T40,'RO=', | D | 38  |
|     | 2F6.3,' INCHES',T59,'NO PTS=',I3/T21,'FLOW RATES')                  | D | 39  |
| 203 | 9 FORMAT (T21,7F8.0)  | D | 40  |
| 204 | END   | D | 41- |
| 205 | SUBROUTINE RECHD  | E | 1   |
|     | C THIS SUBROUTINE RECALLS PREVIOUSLY COMPUTED AND PUNCHED           | E | 2   |
|     | C HYDROGRAPHS   | E | 3   |
| 206 | COMMON CFS(300),OCFS(300,6),IEND(6),DATA(310),DA(6),DP(20),NPU,NHD  | E | 4   |
|     | 1,SCFS(20),C(20),A(20,6),Q(20,6),RAIN(200),DEEP(20,6),NER,MAXNO,NCO | E | 5   |
|     | 2MM,ICC,NCODE,DIST(6),SEGN(6),CTBLE(50,11),ITBLE(50,2),ZALFA(20),DT | E | 6   |
|     | 3(6),TIME,PEAK(6),ROIN,ISG(6)                                       | E | 7   |
| 207 | ID=DATA(1)  | E | 8   |
| 208 | NHD=DATA(2)   | E | 9   |
| 209 | DT(ID)=DATA(3)  | E | 10  |
| 210 | DA(ID)=DATA(4)  | E | 11  |
| 211 | PEAK(ID)=DATA(5)  | E | 12  |
| 212 | ROIN=DATA(6)  | E | 13  |
| 213 | IEND(ID)=DATA(7)  | E | 14  |
| 214 | M=IEND(ID)  | E | 15  |
| 215 | J=8   | E | 16  |

|     |   |   |   |     |
|-----|---|---|---|-----|
| 216 | C | REMAINING DATA ARE FLOW RATES                                       | E | 17  |
| 217 |   | DO 1 I=1,M  | E | 18  |
| 218 | 1 | QCFS(I,ID)=DATA(J)  | E | 19  |
| 219 |   | J=J+1   | E | 20  |
| 220 |   | RETURN  | E | 21  |
|     |   | END   | E | 22- |
| 221 |   | SUBROUTINE CMPHYD   | F | 1   |
|     | C | THIS PROGRAM DEVELOPS A UNIT HYDROGRAPH, CONVERTS MASS RAINFALL     | F | 2   |
|     | C | TO POINT RUNOFF, AND COMPUTES STORM HYDROGRAPHS BY SUMMATION.       | F | 3   |
| 222 |   | COMMON CFS(300),QCFS(300,6),IEND(6),DATA(310),DA(6),DP(20),NPU,NHD  | F | 4   |
|     |   | 1,SCFS(20),C(20),A(20,6),Q(20,6),RAIN(200),DEEP(20,6),NER,MAXNO,NCO | F | 5   |
|     |   | 2MM,ICC,NCODE,DIST(6),SEGN(6),CTBLE(50,11),ITBLE(50,2),ZALFA(20),DT | F | 6   |
|     |   | 3(6),TIME,PEAK(6),ROIN,ISG(6)                                       | F | 7   |
| 223 |   | ID=DATA(1)  | F | 8   |
| 224 |   | NHD=DATA(2)   | F | 9   |
| 225 |   | DT(ID)=DATA(3)  | F | 10  |
| 226 |   | DA(ID)=DATA(4)  | F | 11  |
| 227 |   | CN=DATA(5)  | F | 12  |
|     | C | ARE K AND TP FURNISHED OR WILL THEY BE COMPUTED                     | F | 13  |
| 228 |   | IF (DATA(6)) 1,2,2  | F | 14  |
| 229 | 1 | XK=-DATA(6)   | F | 15  |
| 230 |   | TP=-DATA(7)   | F | 16  |
| 231 |   | GO TO 3   | F | 17  |
| 232 | 2 | HT=DATA(6)  | F | 18  |
| 233 |   | XL=DATA(7)  | F | 19  |
| 234 |   | SLOPE=HT/XL   | F | 20  |
| 235 |   | XLDW=(XL**2.)/DA(ID)  | F | 21  |
| 236 |   | XK=27.0*(DA(ID)**.231)*(SLOPE**(-.777))*(XLDW**.124)                | F | 22  |
| 237 |   | TP=4.63*(DA(ID)**.422)*(SLOPE**(-.46))*(XLDW**.133)                 | F | 23  |
| 238 | 3 | PEAK(ID)=1.   | F | 24  |
| 239 |   | DO 4 I=1,300  | F | 25  |
| 240 | 4 | QCFS(I,ID)=0.   | F | 26  |
|     | C | COMPUTE N BY ITERATION.   | F | 27  |
| 241 |   | XN=5.0  | F | 28  |
| 242 |   | XKTP=XK/TP  | F | 29  |
| 243 |   | DO 6 I=1,50   | F | 30  |
| 244 |   | TINF=1.+SQRT(1./((XN-1.))   | F | 31  |
| 245 |   | XN1=.05/(XKTP*(ALOG(TINF/(TINF+.05))+.05))+1.                       | F | 32  |
| 246 |   | DIFF=ABS(XN1-XN)  | F | 33  |
| 247 |   | IF (DIFF-.001) 7,7,5  | F | 34  |
| 248 | 5 | XN=XN1  | F | 35  |
| 249 | 6 | CONTINUE  | F | 36  |
| 250 |   | WRITE (6,29)  | F | 37  |
| 251 |   | GO TO 28  | F | 38  |
|     | C | DETERMINE C1.   | F | 39  |
| 252 | 7 | DELT=TINF/100.  | F | 40  |
| 253 |   | TC1=0.  | F | 41  |
| 254 |   | XN1P=XN-1.  | F | 42  |
| 255 |   | XN1M=1.-XN  | F | 43  |
| 256 |   | DO 8 I=2,101  | F | 44  |
| 257 |   | TC1=TC1+DELT  | F | 45  |
| 258 | 8 | CFS(I)=(TC1**XN1P)*EXP(XN1M*(TC1-1.))                               | F | 46  |
| 259 |   | SUM=CFS(101)/2.   | F | 47  |
| 260 |   | DO 9 I=2,100  | F | 48  |
| 261 | 9 | SUM=SUM+CFS(I)  | F | 49  |
| 262 |   | C1=SUM*DELT   | F | 50  |
| 263 |   | CFS11=CFS(101)  | F | 51  |
| 264 |   | TTINF=TINF*TP   | F | 52  |
| 265 |   | TREC1=TTINF+2.*XK   | F | 53  |



|     |    |  |   |     |
|-----|----|--|---|-----|
| 266 |    | EEE=EXP((TTINF-TREC1)/XK)                        | F | 54  |
| 267 |    | XK1=3.*XK  | F | 55  |
| 268 |    | B=645.333/(C1+CFSI*(XKTP*(1.-EEE)+EEE*(XK1/TP))) | F | 56  |
|     | C  | COMPUTE B, QP, AND CFSI.                         | F | 57  |
| 269 |    | QP=(B*DA(ID))/TP                                 | F | 58  |
| 270 |    | CFSI=QP*CFS(101)                                 | F | 59  |
| 271 |    | CFSR1=CFSI*EEE                                   | F | 60  |
| 272 |    | WRITE (6,30) XN,QP                               | F | 61  |
|     | C  | DETERMINE INCREMENTAL RUNOFF.                    | F | 62  |
| 273 |    | R=1000./CN-10.                                   | F | 63  |
| 274 |    | B1=.2*R  | F | 64  |
| 275 |    | J=8  | F | 65  |
| 276 |    | IF (DATA(J)) 13,10,10                            | F | 66  |
| 277 | 10 | RAIN(1)=DATA(J)                                  | F | 67  |
| 278 |    | DO 11 I=2,300                                    | F | 68  |
| 279 |    | J=J+1  | F | 69  |
| 280 |    | RAIN(I)=DATA(J)                                  | F | 70  |
| 281 |    | IF (RAIN(I)-RAIN(I-1)) 12,11,11                  | F | 71  |
| 282 | 11 | CONTINUE   | F | 72  |
| 283 | 12 | NUMB=I-1   | F | 73  |
| 284 | 13 | DO 15 I=1,NUMB                                   | F | 74  |
| 285 |    | IF (RAIN(I)-B1) 33,33,14                         | F | 75  |
| 286 | 33 | DATA (I)=0.                                      | F | 76  |
| 287 |    | Q1=0.  | F | 77  |
| 288 |    | GO TO 15   | F | 78  |
| 289 | 14 | Q2=((RAIN(I)-B1)**2.)/(RAIN(I)+.8*R)             | F | 79  |
| 290 |    | DATA (I)=Q2-Q1                                   | F | 80  |
| 291 |    | Q1=Q2  | F | 81  |
| 292 | 15 | CONTINUE   | F | 82  |
|     | C  | COMPUTE UNIT HYDROGRAPH.                         | F | 83  |
| 293 |    | T2=0.  | F | 84  |
| 294 |    | CFS(1)=0.  | F | 85  |
| 295 |    | DO 20 I=2,300                                    | F | 86  |
| 296 |    | T2=T2+DT(ID)                                     | F | 87  |
| 297 |    | IF (T2-TTINF) 16,16,17                           | F | 88  |
| 298 | 16 | CFS(I)=QP*((T2/TP)**XN1P)*EXP(XN1M*(T2/TP-1.))   | F | 89  |
| 299 |    | GO TO 20   | F | 90  |
| 300 | 17 | IF (T2-TREC1) 18,18,19                           | F | 91  |
| 301 | 18 | CFS(I)=CFSI*EXP((TTINF-T2)/XK)                   | F | 92  |
| 302 |    | GO TO 20   | F | 93  |
| 303 | 19 | CFS(I)=CFSR1*EXP((TREC1-T2)/XK1)                 | F | 94  |
| 304 |    | IF (CFS(I)-1.) 21,21,20                          | F | 95  |
| 305 | 20 | CONTINUE   | F | 96  |
| 306 |    | I=300  | F | 97  |
| 307 | 21 | ICND=I   | F | 98  |
|     | C  | COMPUTE STORM HYDROGRAPH.                        | F | 99  |
| 308 |    | DO 24 J=2,NUMB                                   | F | 100 |
| 309 |    | N=J+ICND-2                                       | F | 101 |
| 310 |    | IF (N-300) 23,23,22                              | F | 102 |
| 311 | 22 | N=300  | F | 103 |
| 312 | 23 | KK=J   | F | 104 |
| 313 |    | I=2  | F | 105 |
| 314 |    | DO 24 K=KK,N                                     | F | 106 |
| 315 |    | OCFS(K,ID)=OCFS(K,ID)+DATA(J)*CFS(I)             | F | 107 |
| 316 | 24 | I=I+1  | F | 108 |
| 317 |    | M=K-1  | F | 109 |
| 318 |    | RO=0.  | F | 110 |
| 319 |    | DO 26 I=2,M                                      | F | 111 |
|     | C  | COMPUTE RUNOFF VOLUME                            | F | 112 |
| 320 |    | RO=RO+OCFS(I,ID)                                 | F | 113 |

|     |    |   |        |
|-----|----|---|--------|
|     | C  | DETERMINE PEAK  | F 114  |
| 321 |    | IF (OCFS(I,ID)-PEAK(ID)) 26,26,25   | F 115  |
| 322 | 25 | PEAK(ID)=OCFS(I,ID)   | F 116  |
| 323 | 26 | CONTINUE  | F 117  |
| 324 |    | I=M   | F 118  |
| 325 |    | IEND(ID)=I  | F 119  |
| 326 |    | M=I   | F 120  |
| 327 |    | ROIN=(RO*DT(ID))/(DA(ID)*645.333)   | F 121  |
|     | C  | PUNCH CODE  | F 122  |
| 328 |    | IF (NPU) 28,28,27   | F 123  |
| 329 | 27 | WRITE (7,31) ID,NHD,DT(ID),DA(ID),PEAK(ID),ROIN,IEND(ID)  | F 124  |
| 330 |    | WRITE (7,32) (OCFS(I,ID),I=1,M)   | F 125  |
| 331 | 28 | RETURN  | F 126  |
|     | C  |   | F 127  |
| 332 | 29 | FORMAT('N DID NOT CONVERGE AFTER 50 ITERATIONS.')   | F 128  |
| 333 | 30 | FORMAT(T10,'SHAPE CONSTANT, N = ',F6.3/T10,'UNIT PEAK = ',F10.1,'C<br>IFS'/)  | F 129  |
| 334 | 31 | FORMAT('RECALL HYD',T21,'ID=',I1,T29,'HYD NO=',I3,T42,'DT=',F9.<br>16,' HRS',T61,'DA=',F8.3,' SQ MI'/T21,'PEAK=',F7.0,'CFS',T40,'RO=',<br>2F6.3,' INCHES',T59,'NO PTS=',I3/T21,'FLOW RATES')  | F 130  |
| 335 | 32 | FORMAT (T21,7F8.0)  | F 131  |
| 336 |    | END   | F 132  |
|     |    |   | F 133  |
|     |    |   | F 134- |
| 337 |    | SUBROUTINE PRTHYD   | G 1    |
|     | C  | THIS SUBROUTINE PRINTS THE COORDINATES OF A HYDROGRAPH.   | G 2    |
| 338 |    | COMMON CFS(300),OCFS(300,6),IEND(6),DATA(310),DA(6),DP(20),NPU,NHD<br>1,SCFS(20),C(20),A(20,6),Q(20,6),RAIN(200),DEEP(20,6),NER,MAXNO,NCO<br>2MM,ICC,NCODE,DIST(6),SEGN(6),CTBLE(50,11),ITBLE(50,2),ZALFA(20),DT<br>3(6),TIME,PEAK(6),ROIN,ISG(6) | G 3    |
|     |    | ID=DATA(1)  | G 4    |
| 339 |    |   | G 5    |
| 340 |    | NPK=DATA(2)   | G 6    |
|     | C  | DETERMINE TYPE OF HYDROGRAPH  | G 7    |
| 341 |    | IF (NHD-100) 6,6,2  | G 8    |
| 342 | 1  | WRITE (6,14) NHD  | G 9    |
| 343 |    | GO TO 7   | G 10   |
| 344 | 2  | IF (NHD-300) 3,3,4  | G 11   |
| 345 | 3  | WRITE (6,15) NHD  | G 12   |
| 346 |    | GO TO 7   | G 13   |
| 347 | 4  | IF (NHD-500) 1,1,5  | G 14   |
| 348 | 5  | WRITE (6,16) NHD  | G 15   |
| 349 |    | GO TO 7   | G 16   |
| 350 | 6  | WRITE (6,17) NHD  | G 17   |
|     | C  | POSITIVE NPK MEANS PRINT ONLY PEAK AND VOLUME   | G 18   |
| 351 | 7  | IF (NPK) 8,8,11   | G 19   |
| 352 | 8  | J=0   | G 20   |
| 353 |    | WRITE (6,18)  | G 21   |
| 354 |    | M=IEND(ID)  | G 22   |
| 355 |    | TIME1=TIME  | G 23   |
|     | C  | BUILD TIME ARRAY IN DATA  | G 24   |
| 356 |    | DO 9 I=1,M  | G 25   |
| 357 |    | DATA (I)=TIME1  | G 26   |
| 358 | 9  | TIME1=TIME1+DT(ID)  | G 27   |
| 359 |    | M4=M+4  | G 28   |
| 360 |    | M5=M4/5   | G 29   |
| 361 | 10 | J=J+1   | G 30   |
| 362 |    | WRITE (6,19) (DATA(I),OCFS(I,ID),I=J,M,M5)  | G 31   |
| 363 |    | IF (J-M5) 10,11,11  | G 32   |
| 364 | 11 | WRITE (6,20) ROIN,PEAK(ID)  | G 33   |
| 365 |    | IF (NPU) 13,13,12   | G 34   |
| 366 | 12 | WRITE (7,21) ID,NPK   | G 35   |
|     |    |   | G 36   |
|     |    |   | G 37   |

|     |    |   |   |     |
|-----|----|---|---|-----|
| 367 | 13 | RETURN  | G | 38  |
|     | C  |   | G | 39  |
| 368 | 14 | FORMAT (1H0,46X,21HHYDROGRAPH FROM AREA ,I3/)   | G | 40  |
| 369 | 15 | FORMAT (1H0,41X,19HPARTIAL HYDROGRAPH ,I4/)   | G | 41  |
| 370 | 16 | FORMAT (1H0,39X,29HOUTFLOW HYDROGRAPH RESERVOIR ,I4/)   | G | 42  |
| 371 | 17 | FORMAT (1H0,44X,25HOUTFLOW HYDROGRAPH REACH ,I4/)   | G | 43  |
| 372 | 18 | FORMAT (10X,114HTIME            FLOW            TIME            FLOW                                  | G | 44  |
|     |    | 1TIME            FLOW            TIME            FLOW            TIME            FLOW/1               | G | 45  |
|     |    | 21X,113HHRS            CFS            HRS            CFS            HRS            CFS            HRS | G | 46  |
|     |    | 3 CFS            HRS            CFS            HRS            CFS            HRS                      | G | 47  |
| 373 | 19 | FORMAT (5(5X,F10.3,F10.0))  | G | 48  |
| 374 | 20 | FORMAT (1H0,9X,16HRUNOFF VOLUME = F10.3,8H INCHES /10X,22HPEAK DIS                                    | G | 49  |
|     |    | 1CHARGE RATE = ,F10.1,4H CFS//)   | G | 50  |
| 375 | 21 | WRITE ( 'PRINT HYD',T21,'ID=',I1,T29,'CODE=',I1)  | G | 51  |
| 376 |    | END   | G | 52- |
| 377 |    | SUBROUTINE PUHYD  | H | 1   |
|     | C  | THIS SUBROUTINE PUNCHES HYDROGRAPHS IN FORM TO BE USED BY   | H | 2   |
|     | C  | SUBROUTINE RECHD  | H | 3   |
| 378 |    | COMMON CFS(300),QCFS(300,6),IEND(6),DATA(310),DA(6),DP(20),NPU,NHD                                    | H | 4   |
|     |    | 1,SCFS(20),C(20),A(20,6),Q(20,6),RAIN(200),DEEP(20,6),NER,MAXNO,NCO                                   | H | 5   |
|     |    | 2MM,ICC,NCODE,DIST(6),SEGN(6),CTBLE(50,11),ITBLE(50,2),ZALFA(20),DT                                   | H | 6   |
|     |    | 3(6),TIME,PEAK(6),ROIN,ISG(6)   | H | 7   |
| 379 |    | ID=DATA(1)  | H | 8   |
| 380 |    | M=IEND(ID)  | H | 9   |
| 381 |    | WRITE (7,1) ID,NHD,DT(ID),DA(ID),PEAK(ID),ROIN,IEND(ID)   | H | 10  |
| 382 |    | WRITE (7,2) (QCFS(I,ID),I=1,M)  | H | 11  |
| 383 |    | RETURN  | H | 12  |
|     | C  |   | H | 13  |
| 384 | 1  | FORMAT( 'RECALL HYD',T21,'ID=',I1,T29,'HYD NO=',I3,T42,'DT=',F9.                                      | H | 14  |
|     |    | 16,' HRS',T61,'DA=',F8.3,' SQ MI'/T21,'PEAK=',F7.0,'CFS',T40,'RO=',                                   | H | 15  |
|     |    | 2F6.3,' INCHES',T59,'NO PTS=',I3/T21,'FLOW RATES')  | H | 16  |
| 385 | 2  | FORMAT (T21,7F8.0)  | H | 17  |
| 386 |    | END   | H | 18- |
| 387 |    | SUBROUTINE HPLOT  | I | 1   |
|     | C  | THIS SUBROUTINE PLOTS EITHER 1 OR 2 HYDROGRAPHS ON A SET OF AXIS                                      | I | 2   |
| 388 |    | COMMON CFS(300),QCFS(300,6),IEND(6),DATA(310),DA(6),DP(20),NPU,NHD                                    | I | 3   |
|     |    | 1,SCFS(20),C(20),A(20,6),Q(20,6),RAIN(200),DEEP(20,6),NER,MAXNO,NCO                                   | I | 4   |
|     |    | 2MM,ICC,NCODE,DIST(6),SEGN(6),CTBLE(50,11),ITBLE(50,2),ZALFA(20),DT                                   | I | 5   |
|     |    | 3(6),TIME,PEAK(6),ROIN,ISG(6)   | I | 6   |
| 389 |    | ID1=DATA(1)   | I | 7   |
| 390 |    | ID2=DATA(2)   | I | 8   |
| 391 |    | DATA ZERO, PLUS, BLANK, DASH, DOT/'0','+',',',',','-','.',.'/   | I | 9   |
| 392 |    | MRTO=1  | I | 10  |
| 393 |    | XMRT0=1.  | I | 11  |
| 394 |    | MAX=118   | I | 12  |
| 395 |    | J=1   | I | 13  |
|     | C  | ARE THERE 1 OR 2 HYDROGRAPHS  | I | 14  |
| 396 |    | IF (ID2) 1,1,2  | I | 15  |
|     | C  | DETERMINE HIGHEST PEAK IF 2 HYDROGRAPHS   | I | 16  |
| 397 | 1  | QMAX=PEAK(ID1)  | I | 17  |
| 398 |    | GO TO 14  | I | 18  |
| 399 | 2  | IF (PEAK(ID1)-PEAK(ID2)) 3,3,4  | I | 19  |
| 400 | 3  | QMAX=PEAK(ID2)  | I | 20  |
| 401 |    | GO TO 5   | I | 21  |
| 402 | 4  | QMAX=PEAK(ID1)  | I | 22  |
|     | C  | IF 2 HYDROGRAPHS DETERMINE LARGEST DT AND INTERPOLATE OTHER.  | I | 23  |
|     | C  | HYDROGRAPH IF NECESSARY   | I | 24  |
| 403 | 5  | IF (DT(ID1)-DT(ID2)) 6,13,7   | I | 25  |

|     |    |  |   |    |
|-----|----|--|---|----|
| 404 | 6  | L=ID1  | I | 26 |
| 405 |    | K=ID2  | I | 27 |
| 406 |    | GO TO 8  | I | 28 |
| 407 | 7  | L=ID2'   | I | 29 |
| 408 |    | K=ID1  | I | 30 |
| 409 | 8  | M=IEND(L)  | I | 31 |
| 410 |    | TID=DT(K)  | I | 32 |
| 411 |    | TIDH=0.  | I | 33 |
| 412 |    | DO 11 I=2,M  | I | 34 |
| 413 |    | TIDH=TIDH+DT(L)  | I | 35 |
| 414 |    | IF (TID-TIDH) 10,9,11  | I | 36 |
| 415 | 9  | J=J+1  | I | 37 |
| 416 |    | CFS(J)=OCFS(I,L)   | I | 38 |
| 417 |    | TID=TID+DT(K)  | I | 39 |
| 418 |    | GO TO 11   | I | 40 |
| 419 | 10 | J=J+1  | I | 41 |
| 420 |    | CFS(J)=OCFS(I-1,L)+((TID-TIDH+DT(L))/DT(L))*(OCFS(I,L)-OCFS(I-1,L) | I | 42 |
|     |    | 1)   | I | 43 |
| 421 |    | TID=TID+DT(K)  | I | 44 |
| 422 | 11 | CONTINUE   | I | 45 |
| 423 |    | IEND(L)=J  | I | 46 |
| 424 |    | DT(L)=DT(K)  | I | 47 |
| 425 |    | DO 12 I=2,J  | I | 48 |
| 426 | 12 | OCFS(I,L)=CFS(I)   | I | 49 |
| 427 | 13 | IF (IEND(ID1)-IEND(ID2)) 14,14,15                                  | I | 50 |
| 428 | 14 | M=IEND(ID1)  | I | 51 |
| 429 |    | GO TO 16   | I | 52 |
| 430 | 15 | M=IEND(ID2)  | I | 53 |
| 431 | 16 | IF (M-MAX) 17,17,18  | I | 54 |
|     | C  | DETERMINE TIME SCALE   | I | 55 |
| 432 | 17 | MRTO=MAX/M   | I | 56 |
| 433 |    | XMRTD=MRTO   | I | 57 |
| 434 |    | GO TO 19   | I | 58 |
| 435 | 18 | M=MAX  | I | 59 |
| 436 | 19 | YSCL=QMAX/50.  | I | 60 |
|     | C  | PLOT HYDROGRAPHS   | I | 61 |
| 437 |    | DO 20 I=1,MAX  | I | 62 |
| 438 | 20 | CFS(I)=DASH  | I | 63 |
| 439 |    | WRITE (6,41) QMAX,(CFS(I),I=1,MAX),DOT                             | I | 64 |
| 440 |    | Q1=QMAX  | I | 65 |
| 441 |    | J1=10  | I | 66 |
| 442 |    | DO 37 J=1,50   | I | 67 |
| 443 |    | IF (J-J1) 23,21,23   | I | 68 |
| 444 | 21 | DO 22 I=1,MAX  | I | 69 |
| 445 | 22 | CFS(I)=DASH  | I | 70 |
| 446 |    | GO TO 25   | I | 71 |
| 447 | 23 | DO 24 I=1,MAX  | I | 72 |
| 448 | 24 | CFS(I)=BLANK   | I | 73 |
| 449 | 25 | Q2=Q1-YSCL   | I | 74 |
| 450 |    | K=1  | I | 75 |
| 451 |    | DO 28 I=2,M  | I | 76 |
| 452 |    | K=K+MRTO   | I | 77 |
| 453 |    | IF (OCFS(I,ID1)-Q1) 26,27,28                                       | I | 78 |
| 454 | 26 | IF (OCFS(I,ID1)-Q2) 28,28,27                                       | I | 79 |
| 455 | 27 | CFS(K)=ZERO  | I | 80 |
| 456 | 28 | CONTINUE   | I | 81 |
| 457 |    | WRITE (6,44) DOT,(CFS(I),I=1,MAX),DOT                              | I | 82 |
| 458 |    | IF (ID2) 34,34,29  | I | 83 |
| 459 | 29 | K=1  | I | 84 |
| 460 |    | DO 33 I=2,M  | I | 85 |

|     |    |   |   |      |
|-----|----|---|---|------|
| 461 |    | K=K+MRT0  | I | 86   |
| 462 |    | IF (OCFS(I,ID2)-Q1) 30,31,32  | I | 87   |
| 463 | 30 | IF (OCFS(I,ID2)-Q2) 32,32,31  | I | 88   |
| 464 | 31 | CFS(K)=PLUS   | I | 89   |
| 465 |    | GO TO 33  | I | 90   |
| 466 | 32 | CFS(K)=BLANK  | I | 91   |
| 467 | 33 | CONTINUE  | I | 92   |
| 468 |    | WRITE (6,42) (CFS(I),I=1,MAX)                                       | I | 93   |
| 469 | 34 | IF (J-J1) 36,35,36  | I | 94   |
| 470 | 35 | J1=J1+10  | I | 95   |
| 471 |    | WRITE (6,43) Q2   | I | 96   |
| 472 | 36 | Q1=Q2   | I | 97   |
| 473 | 37 | CONTINUE  | I | 98   |
| 474 |    | CFS(1)=TIME   | I | 99   |
| 475 |    | DTT=DT(ID1)*10./XMRT0   | I | 100  |
|     | C  | PUT TIME ARRAY IN CFS AND WRITE TIME SCALE                          | I | 101  |
| 476 |    | DO 38 I=2,12  | I | 102  |
| 477 | 38 | CFS(I)=CFS(I-1)+DTT   | I | 103  |
| 478 |    | WRITE (6,45) (CFS(I),I=1,12)  | I | 104  |
| 479 |    | WRITE (6,46)  | I | 105  |
| 480 |    | IF (NPU) 40,40,39   | I | 106  |
| 481 | 39 | WRITE (7,47) ID1,ID2  | I | 107  |
| 482 | 40 | RETURN  | I | 108  |
|     | C  |   | I | 109  |
| 483 | 41 | FORMAT(1X,F6.0,' CFS.',119A1)                                       | I | 110  |
| 484 | 42 | FORMAT (1H+,11X,118A1)  | I | 111  |
| 485 | 43 | FORMAT (1H+,F6.0)   | I | 112  |
| 486 | 44 | FORMAT (11X,120A1)  | I | 113  |
| 487 | 45 | FORMAT (6X,12F10.3)   | I | 114  |
| 488 | 46 | FORMAT(49X,'TIME HOURS'///)   | I | 115  |
| 489 | 47 | FORMAT( 'PLOT HYD',T21,'ID I=',I1,T29,'ID II=',I1)                  | I | 116  |
| 490 |    | END   | I | 117- |
| 491 |    | SUBROUTINE ADHYD  | J | 1    |
|     | C  | THIS SUBROUTINE ADDS TWO HYDROGRAPHS.                               | J | 2    |
| 492 |    | COMMON CFS(300),OCFS(300,6),IEND(6),DATA(310),DA(6),DP(20),NPU,NHD  | J | 3    |
|     |    | 1,SCFS(20),C(20),A(20,6),Q(20,6),RAIN(200),DEEP(20,6),NER,MAXNO,NCO | J | 4    |
|     |    | 2MM,ICC,NCODE,DIST(6),SEGN(6),CTBLE(50,11),ITBLE(50,2),ZALFA(20),DT | J | 5    |
|     |    | 3(6),TIME,PEAK(6),ROIN,ISG(6)                                       | J | 6    |
| 493 |    | ID=DATA(1)  | J | 7    |
| 494 |    | NHD=DATA(2)   | J | 8    |
| 495 |    | ID1=DATA(3)   | J | 9    |
| 496 |    | ID2=DATA(4)   | J | 10   |
| 497 |    | PEAK(ID)=1.   | J | 11   |
|     | C  | MAKE TIME INCREMENTS EQUAL IF NOT EQUAL. USE SMALLER INCREMENT      | J | 12   |
| 498 |    | IF (DT(ID1)-DT(ID2)) 1,3,2  | J | 13   |
| 499 | 1  | DT(ID)=DT(ID1)  | J | 14   |
| 500 |    | L=ID1   | J | 15   |
| 501 |    | K=ID2   | J | 16   |
| 502 |    | GO TO 6   | J | 17   |
| 503 | 2  | DT(ID)=DT(ID2)  | J | 18   |
| 504 |    | L=ID2   | J | 19   |
| 505 |    | K=ID1   | J | 20   |
| 506 |    | GO TO 6   | J | 21   |
| 507 | 3  | DT(ID)=DT(ID1)  | J | 22   |
| 508 |    | IF (IEND(ID1)-IEND(ID2)) 4,4,5                                      | J | 23   |
| 509 | 4  | M3=IEND(ID1)  | J | 24   |
| 510 |    | K1=ID2  | J | 25   |
| 511 |    | IEND(ID)=IEND(ID2)  | J | 26   |
| 512 |    | GO TO 18  | J | 27   |

|     |    |  |      |
|-----|----|--|------|
| 513 | 5  | M3=IEND(ID2)   |      |
| 514 |    | K1=ID1   | J 28 |
| 515 |    | IEND(ID)=IEND(ID1)   | J 29 |
| 516 |    | GO TO 18   | J 30 |
|     | C  | DETERMINE DURATIONS OF FLOW  | J 31 |
| 517 | 6  | XIEND1=IEND(ID1)-1   | J 32 |
| 518 |    | XIEND2=IEND(ID2)-1   | J 33 |
| 519 |    | DUR1=XIEND1*DT(ID1)  | J 34 |
| 520 |    | DUR2=XIEND2*DT(ID2)  | J 35 |
| 521 |    | IF (DUR1-DUR2) 7,8,8   | J 36 |
| 522 | 7  | IEND(ID)=DUR2/DT(ID)+1.  | J 37 |
| 523 |    | M3=DUR1/DT(ID)+1.  | J 38 |
| 524 |    | K1=ID2   | J 39 |
| 525 |    | GO TO 9  | J 40 |
| 526 | 8  | IEND(ID)=DUR1/DT(ID)+1.  | J 41 |
| 527 |    | M3=DUR2/DT(ID)+1.  | J 42 |
| 528 |    | K1=ID1   | J 43 |
| 529 | 9  | IF (IEND(ID)-300) 11,11,10   | J 44 |
| 530 | 10 | IEND(ID)=300   | J 45 |
| 531 | 11 | M2=IEND(K)   | J 46 |
| 532 |    | J=1  | J 47 |
|     | C  | INTERPOLATE ONE HYDROGRAPH IF NECESSARY                                | J 48 |
| 533 |    | TIDH=0.  | J 49 |
| 534 |    | TID=DT(ID)   | J 50 |
| 535 |    | DO 15 I=2,M2   | J 51 |
| 536 |    | TIDH=TIDH+DT(K)  | J 52 |
| 537 | 12 | IF (TIDH-TID) 15,13,14   | J 53 |
| 538 | 13 | J=J+1  | J 54 |
| 539 |    | DATA (J)=OCFS(I,K)   | J 55 |
| 540 |    | TID=TID+DT(ID)   | J 56 |
| 541 |    | IF (J-300) 15,16,16  | J 57 |
| 542 | 14 | J=J+1  | J 58 |
| 543 |    | DATA (J)=OCFS(I-1,K)+((TID-TIDH+DT(K))/DT(K))*(OCFS(I,K)-OCFS(I-1,1K)) | J 59 |
| 544 |    | TID=TID+DT(ID)   | J 61 |
| 545 |    | IF (J-300) 12,16,16  | J 62 |
| 546 | 15 | CONTINUE   | J 63 |
| 547 | 16 | IEND(K)=J  | J 64 |
| 548 |    | DO 17 I=2,J  | J 65 |
| 549 | 17 | OCFS(I,K)=DATA(I)  | J 66 |
| 550 | 18 | M=IEND(ID)   | J 67 |
| 551 |    | DA(ID)=DA(ID1)+DA(ID2)   | J 68 |
| 552 |    | RO=0.  | J 69 |
|     | C  | ADD HYDROGRAPHS  | J 70 |
| 553 |    | DO 20 I=1,M3   | J 71 |
| 554 |    | OCFS(I,ID)=OCFS(I,ID1)+OCFS(I,ID2)                                     | J 72 |
| 555 |    | IF (OCFS(I,ID)-PEAK(ID)) 20,20,19                                      | J 73 |
| 556 | 19 | PEAK(ID)=OCFS(I,ID)  | J 74 |
| 557 | 20 | RO=RO+OCFS(I,ID)   | J 75 |
| 558 |    | IF (PEAK(ID)-PEAK(K1)) 21,22,22  | J 76 |
| 559 | 21 | PEAK(ID)=PEAK(K1)  | J 77 |
| 560 | 22 | IF (M-M3) 25,25,23   | J 78 |
| 561 | 23 | M3=M3+1  | J 79 |
| 562 |    | DO 24 I=M3,M   | J 80 |
| 563 |    | OCFS(I,ID)=OCFS(I,K1)  | J 81 |
| 564 | 24 | RO=RO+OCFS(I,ID)   | J 82 |
| 565 | 25 | ROIN=(RO*DT(ID))/(DA(ID)*645.333)                                      | J 83 |
| 566 |    | IF (NPU) 27,27,26  | J 84 |
| 567 | 26 | WRITE (7,28) ID,NHO,ID1,ID2  | J 85 |
| 568 | 27 | RETURN   | J 86 |
|     |    |  | J 87 |

|     |    |   |   |     |
|-----|----|---|---|-----|
| 569 | C  | FORMAT( 'ADD HYD',T21,'ID=',I1,T29,' HYD NO=',I3,T45,'ID I=',I1,    | J | 88  |
|     | 28 | 1T60,'ID II=',I1)   | J | 89  |
| 570 |    | END   | J | 90  |
|     |    |   | J | 91- |
| 571 |    | SUBROUTINE SRC  | K | 1   |
|     | C  | THIS SUBROUTINE STORES AN ELEVATION - END AREA - FLOW TABLE.        | K | 2   |
| 572 |    | COMMON CFS(300),QCFS(300,6),IEND(6),DATA(310),DA(6),DP(20),NPU,NHD  | K | 3   |
|     |    | 1,SCFS(20),C(20),A(20,6),Q(20,6),RAIN(200),DEEP(20,6),NER,MAXNO,NCO | K | 4   |
|     |    | 2MM,ICC,NCODE,DIST(6),SEGN(6),CTBLE(50,11),ITBLE(50,2),ZALFA(20),DT | K | 5   |
|     |    | 3(6),TIME,PEAK(6),ROIN,ISG(6)                                       | K | 6   |
| 573 |    | ID=DATA(1)  | K | 7   |
| 574 |    | VS=DATA(2)  | K | 8   |
|     | C  | VALLEY SECTION NUMBER   | K | 9   |
|     | C  | REMAINING DATA ARE ELEVATION, AREA, AND FLOW FOR EACH POINT OF      | K | 10  |
|     | C  | THE RATING CURVE  | K | 11  |
| 575 |    | EMIN=DATA(3)  | K | 12  |
| 576 |    | J=3   | K | 13  |
| 577 |    | DO 1 I=1,20   | K | 14  |
| 578 |    | ELEV=DATA(J)  | K | 15  |
| 579 |    | DEEP(I,ID)=DATA(J)-EMIN   | K | 16  |
| 580 |    | A(I,ID)=DATA(J+1)   | K | 17  |
| 581 |    | Q(I,ID)=DATA(J+2)   | K | 18  |
| 582 |    | J=J+3   | K | 19  |
| 583 | 1  | CONTINUE  | K | 20  |
| 584 |    | RETURN  | K | 21  |
| 585 |    | END   | K | 22- |
| 586 |    | SUBROUTINE CMPRC  | L | 1   |
|     | C  | THIS SUBROUTINE COMPUTES THE DISCHARGE END-AREA ELEVATION           | L | 2   |
|     | C  | RELATIONSHIP FOR A VALLEY SECTION.                                  | L | 3   |
| 587 |    | COMMON CFS(300),QCFS(300,6),IEND(6),DATA(310),DA(6),DP(20),NPU,NHD  | L | 4   |
|     |    | 1,SCFS(20),C(20),A(20,6),Q(20,6),RAIN(200),DEEP(20,6),NER,MAXNO,NCO | L | 5   |
|     |    | 2MM,ICC,NCODE,DIST(6),SEGN(6),CTBLE(50,11),ITBLE(50,2),ZALFA(20),DT | L | 6   |
|     |    | 3(6),TIME,PEAK(6),ROIN,ISG(6)                                       | L | 7   |
| 588 |    | ID=DATA(1)  | L | 8   |
|     | C  | STORAGE LOCATION NUMBER. (1-6)                                      | L | 9   |
| 589 |    | VS=DATA(2)  | L | 10  |
|     | C  | VALLEY SECTION IDENTIFICATION NUMBER.                               | L | 11  |
| 590 |    | NSEG=DATA(3)  | L | 12  |
|     | C  | NUMBER OF SEGMENTS IN THE VALLEY SECTION.                           | L | 13  |
| 591 |    | ELC=DATA(4)   | L | 14  |
| 592 |    | EMAX=DATA(5)  | L | 15  |
|     | C  | MAXIMUM ELEVATION FOR COMPUTATIONS.                                 | L | 16  |
| 593 |    | SLOPE1=DATA(6)  | L | 17  |
|     | C  | CHANNEL SLOPE.  | L | 18  |
| 594 |    | SLOPE2=DATA(7)  | L | 19  |
|     | C  | FLOOD PLAIN SLOPE.  | L | 20  |
| 595 |    | DIF=(EMAX-ELC)/19.  | L | 21  |
| 596 |    | C(1)=ELO  | L | 22  |
| 597 |    | DO 1 I=2,20   | L | 23  |
| 598 | 1  | C(I)=C(I-1)+DIF   | L | 24  |
|     | C  | SET AREA AND DISCHARGE ARRAYS = 0.                                  | L | 25  |
| 599 |    | DO 2 I=1,20   | L | 26  |
| 600 |    | A(I,ID)=0.  | L | 27  |
| 601 | 2  | Q(I,ID)=0.  | L | 28  |
| 602 |    | J=8   | L | 29  |
| 603 |    | WRITE (6,24) VS   | L | 30  |
|     | C  | READ N VALUES AND SEGMENT BORDER POINTS.                            | L | 31  |
| 604 |    | DO 3 I=1,NSEG   | L | 32  |

|     |    |  |   |    |
|-----|----|--|---|----|
| 605 |    | SEGN(I)=DATA(J)  |   |    |
| 606 |    | DIST(I)=DATA(J+1)  |   |    |
| 607 | 3  | J=J+2  | L | 33 |
|     | C  | REMAINING DATA ITEMS ARE DISTANCES AND ELEVATIONS.             | L | 34 |
| 608 |    | JJJ=J  | L | 35 |
| 609 |    | DO 6 I=1,NSEG  | L | 36 |
| 610 | 4  | J=J+2  | L | 37 |
| 611 |    | IF (DATA(J)-DIST(I)) 4,5,5                                     | L | 38 |
| 612 | 5  | ISG(I)=J+1   | L | 39 |
| 613 | 6  | CONTINUE   | L | 40 |
|     | C  | COMPUTE DISCHARGES AND END AREAS FOR EACH SEGMENT.             | L | 41 |
| 614 |    | DO 22 K=1,NSEG   | L | 42 |
| 615 |    | J=JJJ  | L | 43 |
| 616 |    | JJJ1=JJJ+1   | L | 44 |
| 617 |    | IF (SEGN(K)) 7,7,8   | L | 45 |
| 618 | 7  | SLOPE=SLOPE1   | L | 46 |
| 619 |    | SEGN(K)=-SEGN(K)   | L | 47 |
| 620 |    | GO TO 9  | L | 48 |
| 621 | 8  | SLCPE=SLOPE2   | L | 49 |
| 622 | 9  | SLPN=1.486*SLOPE**.5   | L | 50 |
|     | C  | COMPUTE AREA AND DISCHARGE FOR SEGMENT.                        | L | 51 |
| 623 |    | DO 21 I=2,20   | L | 52 |
| 624 |    | AA=0.  | L | 53 |
| 625 |    | P=0.   | L | 54 |
| 626 |    | J=JJJ-1  | L | 55 |
| 627 |    | DEP2=0.  | L | 56 |
| 628 | 10 | J=J+2  | L | 57 |
| 629 |    | IF (J-ISG(K)) 12,12,11   | L | 58 |
| 630 | 11 | IF (AA-.001) 21,21,20  | L | 59 |
| 631 | 12 | IF (DATA(J)-C(I)) 13,10,10                                     | L | 60 |
| 632 | 13 | DEP1=C(I)-DATA(J)  | L | 61 |
| 633 |    | IF (J-JJJ1) 16,16,14   | L | 62 |
| 634 | 14 | XL=DATA(J-1)-DATA(J-3)   | L | 63 |
| 635 |    | DEP3=ABS(DATA(J-2)-DATA(J))                                    | L | 64 |
| 636 |    | XL=XL*DEP1/DEP3  | L | 65 |
| 637 | 15 | AA=AA+XL*(DEP1+DEP2)/2.  | L | 66 |
| 638 |    | P=P+SQRT((DEP1-DEP2)**2+XL**2)                                 | L | 67 |
| 639 | 16 | DEP2=DEP1  | L | 68 |
| 640 |    | J=J+2  | L | 69 |
| 641 |    | IF (J-ISG(K)) 17,17,20   | L | 70 |
| 642 | 17 | IF (DATA(J)-C(I)) 18,18,19                                     | L | 71 |
| 643 | 18 | DEP1=C(I)-DATA(J)  | L | 72 |
| 644 |    | XL=DATA(J-1)-DATA(J-3)   | L | 73 |
| 645 |    | GO TO 15   | L | 74 |
| 646 | 19 | DEP1=0.  | L | 75 |
| 647 |    | XL=DATA(J-1)-DATA(J-3)   | L | 76 |
| 648 |    | DEP3=ABS(DATA(J-2)-DATA(J))                                    | L | 77 |
| 649 |    | XL=XL*DEP2/DEP3  | L | 78 |
| 650 |    | AA=AA+XL*(DEP1+DEP2)/2.  | L | 79 |
| 651 |    | P=P+SQRT((DEP1-DEP2)**2+XL**2)                                 | L | 80 |
| 652 |    | DEP2=0.  | L | 81 |
| 653 |    | GO TO 10   | L | 82 |
| 654 | 20 | R=AA/P   | L | 83 |
| 655 |    | SGN=SEGN(K)-.0025*R  | L | 84 |
|     | C  | ADD DISCHARGES AND AREAS FOR ALL SEGMENTS TO OBTAIN TOTALS FOR | L | 85 |
|     | C  | VALLEY SECTION.  | L | 86 |
| 656 |    | Q(I,ID)=Q(I,ID)+AA*R**.66667*SLPN/SGN                          | L | 87 |
| 657 |    | A(I,ID)=A(I,ID)+AA   | L | 88 |
| 658 | 21 | CONTINUE   | L | 89 |
| 659 |    | JJJ=J-3  | L | 90 |
|     |    |  | L | 91 |
|     |    |  | L | 92 |



|     |    |   |   |      |
|-----|----|---|---|------|
| 660 | 22 | CONTINUE  | L | 93   |
| 661 |    | DO 23 I=1,20  | L | 94   |
| 662 |    | DEEP(I,ID)=C(I)-ELD   | L | 95   |
| 663 |    | WRITE (6,25) C(I),A(I,ID),Q(I,ID)   | L | 96   |
| 664 | 23 | CONTINUE  | L | 97   |
| 665 |    | RETURN  | L | 98   |
|     | C  |   | L | 99   |
| 666 | 24 | FORMAT(1H0,T42,'RATING CURVE VALLEY SECTION',F5.1/T46,'WATER',T56,<br>1'FLOW',T66,'FLOW'/T45,'SURFACE',T56,'AREA',T66,'RATE'/T46,'ELEV',T<br>256,'SQ FT',T66,'CFS') | L | 100  |
|     |    |   | L | 101  |
|     |    |   | L | 102  |
| 667 | 25 | FORMAT (40X,F10.2,2F10.1)   | L | 103  |
| 668 |    | END   | L | 104- |
| 669 |    | SUBROUTINE STT  | M | 1    |
|     | C  | THIS SUBROUTINE STORES A DEPTH - FLOW - TRAVEL TIME TABLE.  | M | 2    |
| 670 |    | COMMON CFS(300),QCFS(300,6),IEND(6),DATA(310),DA(6),DP(20),NPU,NHD  | M | 3    |
|     |    | 1,SCFS(20),C(20),A(20,6),Q(20,6),RAIN(200),DEEP(20,6),NER,MAXNO,NCO   | M | 4    |
|     |    | 2MM,ICC,NCODE,DIST(6),SEGN(6),CTBLE(50,11),ITBLE(50,2),ZALFA(20),DT   | M | 5    |
|     |    | 3(6),TIME,PEAK(6),ROIN,ISG(6)   | M | 6    |
| 671 |    | ID=DATA(1)  | M | 7    |
| 672 |    | REACH=DATA(2)   | M | 8    |
| 673 |    | XL=DATA(3)  | M | 9    |
| 674 |    | SLOPE=DATA(4)   | M | 10   |
| 675 |    | DIST(ID)=SLOPE*XL   | M | 11   |
| 676 |    | J=5   | M | 12   |
| 677 |    | DO 1 I=1,19   | M | 13   |
| 678 |    | DP(I)=DATA(J)   | M | 14   |
| 679 |    | SCFS(I)=DATA(J+1)   | M | 15   |
| 680 |    | C(I)=DATA(J+2)  | M | 16   |
| 681 | 1  | J=J+3   | M | 17   |
| 682 |    | RETURN  | M | 18   |
| 683 |    | END   | M | 19-  |
| 684 |    | SUBROUTINE CMPTT  | N | 1    |
|     | C  | THIS SUBROUTINE COMPUTES THE TRAVEL TIME AT GIVEN   | N | 2    |
|     | C  | DISCHARGE RATES   | N | 3    |
| 685 |    | COMMON CFS(300),QCFS(300,6),IEND(6),DATA(310),DA(6),DP(20),NPU,NHD  | N | 4    |
|     |    | 1,SCFS(20),C(20),A(20,6),Q(20,6),RAIN(200),DEEP(20,6),NER,MAXNO,NCO   | N | 5    |
|     |    | 2MM,ICC,NCODE,DIST(6),SEGN(6),CTBLE(50,11),ITBLE(50,2),ZALFA(20),DT   | N | 6    |
|     |    | 3(6),TIME,PEAK(6),ROIN,ISG(6)   | N | 7    |
| 686 |    | ID=DATA(1)  | N | 8    |
| 687 |    | REACH=DATA(2)   | N | 9    |
| 688 |    | NOVS=DATA(3)  | N | 10   |
| 689 |    | XL=DATA(4)  | N | 11   |
| 690 |    | SLOPE=DATA(5)   | N | 12   |
| 691 |    | DIST(ID)=SLOPE*XL   | N | 13   |
| 692 |    | XLD36=XL/3600.  | N | 14   |
|     | C  | ZERO ARRAYS   | N | 15   |
| 693 |    | DO 1 J=1,20   | N | 16   |
| 694 |    | DATA (J)=0.   | N | 17   |
| 695 | 1  | CFS(J)=0.   | N | 18   |
| 696 |    | ID1=1   | N | 19   |
|     | C  | FIND RATING CURVE WITH SMALLEST MAXIMUM FLOW RATE   | N | 20   |
| 697 | 2  | QMIN=Q(20,ID1)  | N | 21   |
| 698 |    | MIN=ID1   | N | 22   |
| 699 |    | GO TO 4   | N | 23   |
| 700 | 3  | ID1=ID1+1   | N | 24   |
| 701 |    | IF (QMIN-Q(20,ID1)) 4,4,2   | N | 25   |
| 702 | 4  | IF (ID1-NOVS) 3,5,5   | N | 26   |
| 703 | 5  | I=1   | N | 27   |

|     |    |   |   |     |
|-----|----|---|---|-----|
| 704 | C  | SET SCFS ARRAY EQUAL TO Q ARRAY OF LOWEST RATING CURVE              | N | 28  |
| 705 |    | DO 6 J=2,20   | N | 29  |
| 706 | 6  | SCFS(I)=Q(J,MIN)  | N | 30  |
|     |    | I=I+1   | N | 31  |
| 707 | C  | COMPUT END AREA AND DEPTH   | N | 32  |
| 708 |    | DO 9 ID1=1,NOVS   | N | 33  |
| 709 |    | DO 9 J=1,19   | N | 34  |
| 710 |    | DO 7 I=2,20   | N | 35  |
| 711 |    | IF (Q(I,ID1)-SCFS(J)) 7,17,8  | N | 36  |
| 712 | 7  | CONTINUE  | N | 37  |
| 713 | 17 | DATA (J)=A(I,ID1)+DATA(J)   | N | 38  |
| 714 |    | CFS(J)=DEEP(I,ID1)+CFS(J)   | N | 39  |
| 715 |    | GO TO 9   | N | 40  |
| 716 | 8  | XY=(SCFS(J)-Q(I-1,ID1))/(Q(I,ID1)-Q(I-1,ID1))                       | N | 41  |
| 717 |    | DATA (J)=A(I-1,ID1)+XY*(A(I,ID1)-A(I-1,ID1))+DATA(J)                | N | 42  |
| 718 | 9  | CFS(J)=DEEP(I-1,ID1)+XY*(DEEP(I,ID1)-DEEP(I-1,ID1))+CFS(J)          | N | 43  |
| 719 |    | CONTINUE  | N | 44  |
| 720 |    | XNCVS=NOVS  | N | 45  |
|     |    | WRITE (6,13) REACH  | N | 46  |
|     | C  | COMPUTE TRAVEL TIME   | N | 47  |
| 721 |    | DO 10 I=1,19  | N | 48  |
| 722 |    | AVAREA=DATA(I)/XNOVS  | N | 49  |
| 723 |    | DP(I)=CFS(I)/XNOVS  | N | 50  |
| 724 |    | S=AVAREA*XL036  | N | 51  |
| 725 |    | C(I)=S/SCFS(I)  | N | 52  |
| 726 |    | WRITE (6,14) DP(I),SCFS(I),C(I)                                     | N | 53  |
| 727 | 10 | CONTINUE  | N | 54  |
|     | C  | PUNCH CODE  | N | 55  |
| 728 |    | IF (NPU) 12,12,11   | N | 56  |
| 729 | 11 | WRITE (7,15) ID,REACH,XL,SLOPE                                      | N | 57  |
| 730 |    | WRITE (7,16) (DP(I),SCFS(I),C(I),I=1,19)                            | N | 58  |
| 731 | 12 | RETURN  | N | 59  |
|     | C  |   | N | 60  |
| 732 | 13 | FORMAT(1H0,T46,'TRAVEL TIME TABLE'/T54,'REACH',F5.1/T46,'WATER',T   | N | 61  |
|     |    | 156,'FLOW',T65,'TRAVEL'/T46,'DEPTH',T56,'RATE',T66,'TIME'/T46,'FEET | N | 62  |
|     |    | 2',T56,'CFS',T66,'HRS')   | N | 63  |
| 733 | 14 | FORMAT (40X,F10.2,F10.0,F10.4)                                      | N | 64  |
| 734 | 15 | FORMAT('STORE TRAVEL TIME',T21,'ID=',I1,T29,'REACH NO=',F5.1,T44,   | N | 65  |
|     |    | 1,'LENGTH=',F9.0,' FT'/T21,'SLOPE=',F8.6,'FT/FT'                    | N | 66  |
|     |    | 21,'DEPTH(FT)',T35,'FLOW(CFS)',T49,'TIME(HRS)')/T2                  | N | 67  |
| 735 | 16 | FORMAT (T21,F7.2,F15.0,F15.3)                                       | N | 68  |
| 736 |    | END   | N | 69- |
| 737 |    | SUBROUTINE ROUTE  | O | 1   |
|     | C  | THIS SUBROUTINE ROUTES A HYDROGRAPH THROUGH A REACH WITH THE        | O | 2   |
|     | C  | NEW VSC METHOD OF FLOOD ROUTING. THIS METHOD ACCOUNTS FOR THE       | O | 3   |
|     | C  | VARIATION IN WATER SURFACE SLOPE.                                   | O | 4   |
| 738 |    | COMMON CFS(300),DCFS(300,6),IEND(6),DATA(310),DA(6),DP(20),NPU,NHD  | O | 5   |
|     |    | 1,SCFS(20),C(20),A(20,6),Q(20,6),RAIN(200),DEEP(20,6),NER,MAXNO,NCO | O | 6   |
|     |    | 2MM,ICC,NCODE,DIST(6),SEGN(6),CTBLE(50,11),ITBLE(50,2),ZALFA(20),DT | O | 7   |
|     |    | 3(6),TIME,PEAK(6),ROIN,ISG(6)                                       | O | 8   |
| 739 |    | ID=DATA(1)  | O | 9   |
| 740 |    | NHD=DATA(2)   | O | 10  |
| 741 |    | IDH=DATA(3)   | O | 11  |
| 742 |    | DT(ID)=DATA(4)  | O | 12  |
| 743 |    | DA(ID)=DA(IDH)  | O | 13  |
| 744 |    | M=IEND(IDH)   | O | 14  |
|     | C  | IF ID AND IDH ARE EQUAL, ADD 1 TO IDH                               | O | 15  |
| 745 |    | IF (ID-IDH) 3,1,3   | O | 16  |
| 746 | 1  | IDH=IDH+1   | O | 17  |

```

747      DO 2 I=1,M
748 2      OCFS(I,IDH)=OCFS(I,IDH-1)
749      DT(IDH)=DT(IDH-1)
750      PEAK(IDH)=PEAK(IDH-1)
751 3      NERRT=0
752      PEAK(ID)=1.
753      RO=0.
754      N=19
755      OCFS(1,ID)=0.
756      S=0.
757      T1=C(1)
758      J=1
759      GUES=1.
760      CFS(1)=0.
      C      IF ROUTING INTERVAL IS NOT EQUAL TO TIME INCREMENT OF INFLOW
      C      HYDROGRAPH, INTERPOLATE
761      IF (DT(ID)-DT(IDH)) 8,15,4
762 4      TID=DT(ID)
763      TIDH=0.
764      DO 7 I=2,M
765      TIDH=TIDH+DT(IDH)
766      IF (TID-TIDH) 6,5,7
767 5      J=J+1
768      CFS(J)=OCFS(I,IDH)
769      TID=TID+DT(ID)
770      GO TO 7
771 6      J=J+1
772      CFS(J)=OCFS(I-1,IDH)+((TID-TIDH+DT(IDH))/DT(IDH))*(OCFS(I,IDH)-OC
1S(I-1,IDH))
773      TID=TID+DT(ID)
774 7      CONTINUE
775      GO TO 13
776 8      TIDH=0.
777      TID=DT(ID)
778      DO 12 I=2,M
779      TIDH=TIDH+DT(IDH)
780 9      IF (TIDH-TID) 12,10,11
781 10      J=J+1
782      CFS(J)=OCFS(I,IDH)
783      TID=TID+DT(ID)
784      IF (J-300) 12,13,13
785 11      J=J+1
786      CFS(J)=OCFS(I-1,IDH)+((TID-TIDH+DT(IDH))/DT(IDH))*(OCFS(I,IDH)-OC
1S(I-1,IDH))
787      TID=TID+DT(ID)
788      IF (J-300) 9,13,13
789 12      CONTINUE
790 13      IEND(IDH)=J
791      DT(IDH)=DT(ID)
792      M=J
793      DO 14 I=2,M
794 14      OCFS(I,IDH)=CFS(I)
      C      IF INFLOW IS ZERO, SO IS OUTFLOW
795 15      DO 16 L=2,M
796      IF (OCFS(L,IDH)) 16,16,49
797 16      OCFS(L,ID)=0.
      C      ROUTE
798 49      DATA (L-1)=0.
799      DO 42 I=L,300
800      IF (I-M) 18,18,17

```

|     |    |   |       |
|-----|----|---|-------|
| 801 | 17 | OCFS(I,IDH)=OCFS(I-1,IDH)*.9                      |       |
| 802 | 18 | AVIN=(OCFS(I,IDH)+OCFS(I-1,IDH))/2.               | 0 78  |
| 803 |    | SIA=S+AVIN  | 0 79  |
| 804 |    | J=1   | 0 80  |
|     | C  | DETERMINE DEPTH AND TRAVEL TIME OF INFLOW         | 0 81  |
| 805 |    | IF (OCFS(I,IDH)-SCFS(1)) 19,23,20                 | 0 82  |
| 806 | 19 | DI2=(OCFS(I,IDH)/SCFS(1))*DP(1)                   | 0 83  |
| 807 |    | TI2=C(1)  | 0 84  |
| 808 |    | GO TO 25  | 0 85  |
| 809 | 20 | DO 21 J=2,N                                       | 0 86  |
| 810 |    | IF (OCFS(I,IDH)-SCFS(J)) 24,23,21                 | 0 87  |
| 811 | 21 | CONTINUE  | 0 88  |
| 812 |    | IF (NERRT) 22,22,36                               | 0 89  |
| 813 | 22 | WRITE (6,46)                                      | 0 90  |
| 814 |    | NERRT=1   | 0 91  |
| 815 |    | GO TO 36  | 0 92  |
| 816 | 23 | DI2=DP(J)   | 0 93  |
| 817 |    | TI2=C(J)  | 0 94  |
| 818 |    | GO TO 25  | 0 95  |
| 819 | 24 | RATIO=(OCFS(I,IDH)-SCFS(J-1))/(SCFS(J)-SCFS(J-1)) | 0 96  |
| 820 |    | DI2=DP(J-1)+RATIO*(DP(J)-DP(J-1))                 | 0 97  |
| 821 |    | TI2=C(J-1)+RATIO*(C(J)-C(J-1))                    | 0 98  |
| 822 | 25 | DO 35 IT=1,10                                     | 0 99  |
| 823 |    | J=1   | 0 100 |
|     | C  | DETERMINE DEPTH AND TRAVEL TIME OF OUTFLOW        | 0 101 |
| 824 |    | IF (GUES-SCFS(1)) 26,29,27                        | 0 102 |
| 825 | 26 | DO2=(GUES/SCFS(1))*DP(1)                          | 0 103 |
| 826 |    | TO2=C(1)  | 0 104 |
| 827 |    | GO TO 31  | 0 105 |
| 828 | 27 | DO 28 J=2,N                                       | 0 106 |
| 829 |    | IF (GUES-SCFS(J)) 30,29,28                        | 0 107 |
| 830 | 28 | CONTINUE  | 0 108 |
| 831 |    | J=N   | 0 109 |
| 832 | 29 | DO2=DP(J)   | 0 110 |
| 833 |    | TO2=C(J)  | 0 111 |
| 834 |    | GO TO 31  | 0 112 |
| 835 | 30 | RATIO=(GUES-SCFS(J-1))/(SCFS(J)-SCFS(J-1))        | 0 113 |
| 836 |    | DO2=DP(J-1)+RATIO*(DP(J)-DP(J-1))                 | 0 114 |
| 837 |    | TO2=C(J-1)+RATIO*(C(J)-C(J-1))                    | 0 115 |
|     | C  | FIND WATER SURFACE SLOPE                          | 0 116 |
| 838 | 31 | DDD=DI2/(DI2+DO2)                                 | 0 117 |
| 839 |    | IF (DDD-.01) 32,32,33                             | 0 118 |
| 840 | 32 | GUES=OCFS(I-1,IDH)                                | 0 119 |
| 841 |    | GO TO 35  | 0 120 |
| 842 | 33 | T2=.5*(TI2+TO2)                                   | 0 121 |
| 843 |    | T2=T2*SQRT(DDD)                                   | 0 122 |
| 844 |    | T=TI2+T2  | 0 123 |
|     | C  | COMPUTE ROUTING COEFFICIENT                       | 0 124 |
| 845 |    | COEF=(2.*DT(ID))/(T+DT(ID))                       | 0 125 |
| 846 |    | O2=COEF*SIA                                       | 0 126 |
| 847 |    | TRY1=GUES   | 0 127 |
| 848 |    | RATIO=O2/(GUES+.1E-20)                            | 0 128 |
| 849 |    | DIFF=ABS(1.-RATIO)                                | 0 129 |
|     | C  | TEST FOR CONVERGENCE                              | 0 130 |
| 850 |    | IF (DIFF-.001) 37,37,34                           | 0 131 |
| 851 | 34 | GUES=O2   | 0 132 |
| 852 | 35 | CONTINUE  | 0 133 |
| 853 |    | OCFS(I,ID)=DATA(I-1)*SIA                          | 0 134 |
| 854 |    | DATA (I)=DATA(I-1)                                | 0 135 |
| 855 |    | WRITE (6,47) I,OCFS(I,ID)                         | 0 136 |
|     |    |   | 0 137 |

|     |    |  |                         |
|-----|----|--|-------------------------|
| 856 |    | GO TO 38   | O 138                   |
| 857 | 36 | OCFS(I,ID)=DATA(I-1)*SIA   | O 139                   |
| 858 |    | DATA(I)=DATA(I-1)  | O 140                   |
| 859 |    | GO TO 38   | O 141                   |
| 860 | 37 | OCFS(I,ID)=O2  | O 142                   |
| 861 |    | DATA(I)=COEF   | O 143                   |
|     | C  | COMPUTE NEW STORAGE  | O 144                   |
| 862 | 38 | S=SIA-OCFS(I,ID)   | O 145                   |
| 863 |    | T1=T2  | O 146                   |
| 864 |    | RO=RO+OCFS(I,ID)   | O 147                   |
| 865 |    | IF (OCFS(I,ID)-OCFS(I-1,ID)) 39,40,40  | O 148                   |
| 866 | 39 | IF (OCFS(I,ID)-1.) 43,43,42  | O 149                   |
| 867 | 40 | IF (OCFS(I,ID)-PEAK(ID)) 42,42,41  | O 150                   |
| 868 | 41 | PEAK(ID)=OCFS(I,ID)  | O 151                   |
| 869 | 42 | CONTINUE   | O 152                   |
| 870 |    | I=300  | O 153                   |
| 871 | 43 | IEND(ID)=I   | O 154                   |
| 872 |    | ROIN=(RO*DT(ID))/(DA(ID)*645.333)  | O 155                   |
|     | C  | PUNCH CODE   | O 156                   |
| 873 |    | IF (NPU) 45,45,44  | O 157                   |
| 874 | 44 | WRITE (7,48) ID,NHD,IDH,DT(ID)   | O 158                   |
| 875 | 45 | RETURN   | O 159                   |
|     | C  |  | O 160                   |
| 876 | 46 | FORMAT(IHO,'TRAVEL TIME TABLE EXCEEDED')   | O 161                   |
| 877 | 47 | FORMAT(TIO,'PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERG<br>IENCE WAS FORCED.//T20,'OUTFLOW NUMBER = ',I4,'RATE =',F10.2) | O 162                   |
| 878 | 48 | FORMAT( 'ROUTE',T21,'ID=',I1,T29,'HYD NO=',I3,T45,'INFLOW ID=',I<br>11,T65,'DT=',F8.6,'HRS')   | O 163<br>O 164<br>O 165 |
| 879 |    | END  | O 166-                  |
| 880 |    | SUBROUTINE RESVO   | P 1                     |
|     | C  | THIS SUBROUTINE ROUTES A HYDROGRAPH THROUGH A RESERVOIR WITH THE   | P 2                     |
|     | C  | STORAGE-INDICATION METHOD.   | P 3                     |
| 881 |    | COMMON CFS(300),OCFS(300,6),IEND(6),DATA(310),DA(6),DP(20),NPU,NHD   | P 4                     |
|     |    | 1,SCFS(20),C(20),A(20,6),Q(20,6),RAIN(200),DEEP(20,6),NER,MAXNO,NCO  | P 5                     |
|     |    | 2MM,ICC,NCODE,DIST(6),SEGN(6),CTBLE(50,11),ITBLE(50,2),ZALFA(20),DT  | P 6                     |
|     |    | 3(6),TIME,PEAK(6),ROIN,ISG(6)  | P 7                     |
| 882 |    | ID=DATA(1)   | P 8                     |
| 883 |    | NHD=DATA(2)  | P 9                     |
| 884 |    | IDH=DATA(3)  | P 10                    |
| 885 |    | NERES=0  | P 11                    |
| 886 |    | DT(ID)=DT(IDH)   | P 12                    |
| 887 |    | RO=0.  | P 13                    |
| 888 |    | DA(ID)=DA(IDH)   | P 14                    |
| 889 |    | PEAK(ID)=1.  | P 15                    |
| 890 |    | J=1  | P 16                    |
| 891 |    | I=4  | P 17                    |
|     | C  | REMAINING DATA ARE FLOW AND STORAGE VALUES   | P 18                    |
| 892 |    | SCFS(J)=DATA(I)  | P 19                    |
| 893 |    | STORE=DATA(I+1)*12.1   | P 20                    |
| 894 |    | STORE=STORE1   | P 21                    |
|     | C  | COMPUTE STORAGE COEFFICIENT ARRAY C  | P 22                    |
| 895 | 1  | C(J)=(SCFS(J)/2.)+(STORE/DT(ID))   | P 23                    |
| 896 |    | I=I+2  | P 24                    |
| 897 |    | J=J+1  | P 25                    |
| 898 |    | IF (J-20) 2,2,3  | P 26                    |
| 899 | 2  | SCFS(J)=DATA(I)  | P 27                    |
| 900 |    | STORE=DATA(I+1)*12.1   | P 28                    |
| 901 |    | IF (SCFS(J)-.001) 3,3,1  | P 29                    |
| 902 | 3  | N=J-1  | P 30                    |

|     |    |  |   |     |
|-----|----|--|---|-----|
| 903 |    | OCFS(1,10)=0.  |   |     |
| 904 |    | S=STORE1/DT(IG)  | P | 31  |
|     | C  | ROUTE  | P | 32  |
| 905 |    | DO 15 I=2,150  | P | 33  |
| 906 |    | IF (I-IEND(IDH)) 5,5,4   | P | 34  |
| 907 | 4  | OCFS(I,IDH)=0.0  | P | 35  |
| 908 | 5  | AVIN=(OCFS(I,IDH)+OCFS(I-1,IDH))/2.  | P | 36  |
| 909 |    | SIA=S+AVIN   | P | 37  |
|     | C  | DETERMINE PROPER C   | P | 38  |
| 910 |    | DO 6 J=1,N   | P | 39  |
| 911 |    | IF (SIA-C(J)) 10,9,6   | P | 40  |
| 912 | 6  | CONTINUE   | P | 41  |
| 913 |    | IF (NERES) 7,7,8   | P | 42  |
| 914 | 7  | WRITE (6,19)   | P | 43  |
| 915 |    | NERES=1  | P | 44  |
| 916 | 8  | RESC=SCFS(N)/C(N)  | P | 45  |
|     | C  | COMPUT OUTFLOW   | P | 46  |
| 917 |    | OCFS(I,ID)=RESC*SIA  | P | 47  |
| 918 |    | GO TO 11   | P | 48  |
| 919 | 9  | OCFS(I,ID)=SCFS(J)   | P | 49  |
| 920 |    | GO TO 11   | P | 50  |
| 921 | 10 | OCFS(I,ID)=SCFS(J-1)+((SIA-C(J-1))/(C(J)-C(J-1)))*(SCFS(J)-SCFS(J-1))  | P | 51  |
|     | C  | DETERMINE NEW STORAGE  | P | 52  |
| 922 | 11 | S=SIA-OCFS(I,ID)   | P | 53  |
| 923 |    | RO=RO+OCFS(I,ID)   | P | 54  |
| 924 |    | IF (OCFS(I,ID)-OCFS(I-1,ID)) 12,13,13  | P | 55  |
| 925 | 12 | IF (OCFS(I,ID)-1.) 16,16,15  | P | 56  |
| 926 | 13 | IF (OCFS(I,ID)-PEAK(ID)) 15,15,14  | P | 57  |
| 927 | 14 | PEAK(ID)=OCFS(I,ID)  | P | 58  |
| 928 | 15 | CONTINUE   | P | 59  |
| 929 |    | I=150  | P | 60  |
| 930 | 16 | IFND(ID)=1   | P | 61  |
| 931 |    | ROIN=RO*DT(ID)/(DA(ID)*645.333)  | P | 62  |
|     | C  | PUNCH CODE   | P | 63  |
| 932 |    | IF (NPU) 18,18,17  | P | 64  |
| 933 | 17 | WRITE (7,20) ID,NHD,IDH  | P | 65  |
| 934 |    | II=2*N+3   | P | 66  |
| 935 |    | WRITE (7,21) (DATA(I),I=5,II)  | P | 67  |
| 936 | 18 | RETURN   | P | 68  |
|     | C  |  | P | 69  |
| 937 | 19 | FORMAT (1H0,33HSTORAGE-DISCHARGE TABLE EXCEEDED.)  | P | 70  |
| 938 | 20 | FORMAT('ROUTE RESERVOIR',T21,'ID=',I1,T29,'HYD NO=',I3,T42,'INF<br>1LOW ID=',I1 /T21,'OUTFLOW(CFS)',T37,'STOR<br>2AGE(AC FT)') | P | 71  |
| 939 | 21 | FORMAT (T21,F10.1,F13.1)   | P | 72  |
| 940 |    | END  | P | 73  |
|     |    |  | P | 74  |
|     |    |  | P | 75  |
|     |    |  | P | 76- |
| 941 |    | SUBROUTINE ERROR   | Q | 1   |
|     | C  | THIS SUBROUTINE DETERMINES THE ERROR STANDARD DEVIATION AND THE  | Q | 2   |
|     | C  | PEAK FLOW ERROR FOR 2 HYDROGRAPHS  | Q | 3   |
| 942 |    | COMMON CFS(300),OCFS(300,6),IEND(6),DATA(310),DA(6),DP(20),NPU,NHD   | Q | 4   |
|     |    | 1,SCFS(20),C(20),A(20,6),Q(20,6),RAIN(200),DEEP(20,6),NER,MAXNO,NCO  | Q | 5   |
|     |    | 2MM,ICC,NCODE,DIST(6),SEGN(6),CTOLE(50,11),ITBLE(50,2),ZALFA(20),DT  | Q | 6   |
|     |    | 3(6),TIME,PEAK(6),ROIN,ISG(6)  | Q | 7   |
| 943 |    | ID1=DATA(1)  | Q | 8   |
| 944 |    | ID2=DATA(2)  | Q | 9   |
| 945 |    | SSE=0.   | Q | 10  |
| 946 |    | WRITE (6,15)   | Q | 11  |
| 947 |    | J=1  | Q | 12  |

|     |    |   |   |     |
|-----|----|---|---|-----|
| 948 | C  | IF TIME INCREMENTS NOT EQUAL, INTERPOLATE                           | Q | 13  |
| 949 | 1  | IF (DT(ID1)-DT(ID2)) 1,8,2  | Q | 14  |
| 950 |    | L=ID1   | Q | 15  |
| 951 |    | K=ID2   | Q | 16  |
| 952 | 2  | GO TO 3   | Q | 17  |
| 953 |    | L=ID2   | Q | 18  |
| 954 | 3  | K=ID1   | Q | 19  |
| 955 |    | M=IEND(L)   | Q | 20  |
| 956 |    | TID=DT(K)   | Q | 21  |
| 957 |    | TIDH=0.   | Q | 22  |
| 958 |    | DO 6 I=2,M  | Q | 23  |
| 959 |    | TIDH=TIDH+DT(L)   | Q | 24  |
| 960 | 4  | IF (TID-TIDH) 5,4,6   | Q | 25  |
| 961 |    | J=J+1   | Q | 26  |
| 962 |    | CFS(J)=OCFS(I,L)  | Q | 27  |
| 963 |    | TID=TID+DT(K)   | Q | 28  |
| 964 | 5  | GO TO 6   | Q | 29  |
| 965 |    | J=J+1   | Q | 30  |
|     |    | CFS(J)=OCFS(I-1,L)+((TID-TIDH+DT(L))/DT(L))*(OCFS(I,L)-OCFS(I-1,L)) | Q | 31  |
| 966 |    | 1)  | Q | 32  |
| 967 | 6  | TIC=TID+DT(K)   | Q | 33  |
| 968 |    | CONTINUE  | Q | 34  |
| 969 |    | IEND(L)=J   | Q | 35  |
| 970 |    | DT(L)=DT(K)   | Q | 36  |
| 971 | 7  | DO 7 I=2,J  | Q | 37  |
| 972 | 8  | OCFS(I,L)=CFS(I)  | Q | 38  |
| 973 | 9  | IF (IEND(ID1)-IEND(ID2)) 9,9,10                                     | Q | 39  |
| 974 |    | M=IEND(ID1)   | Q | 40  |
| 975 | 10 | GO TO 11  | Q | 41  |
| 976 | 11 | M=IEND(ID2)   | Q | 42  |
|     |    | T2=TIME   | Q | 43  |
| 977 | C  | DETERMINE ERROR   | Q | 44  |
| 978 |    | DO 12 I=1,M   | Q | 45  |
| 979 |    | ERR=OCFS(I,ID1)-OCFS(I,ID2)   | Q | 46  |
| 980 |    | WRITE (6,16) T2,OCFS(I,ID1),OCFS(I,ID2),ERR                         | Q | 47  |
|     |    | T2=T2+DT(ID1)   | Q | 48  |
| 981 | C  | SUM OF SQUARES OF ERROR   | Q | 49  |
| 982 | 12 | SSE=SSE+ERR*ERR   | Q | 50  |
|     |    | XM=M  | Q | 51  |
| 983 | C  | ERROR VARIANCE  | Q | 52  |
|     |    | EVAR=SSE/XM   | Q | 53  |
| 984 | C  | ERROR STANDARD DEVIATION  | Q | 54  |
| 985 |    | ESDEV=SQRT(EVAR)  | Q | 55  |
|     |    | WRITE (6,17) ESDEV  | Q | 56  |
| 986 | C  | PERCENT ERROR FOR PEAK FLOWS  | Q | 57  |
| 987 |    | ERPK=ABS(PEAK(ID1)-PEAK(ID2))                                       | Q | 58  |
| 988 |    | PCTER=(ERPK/PEAK(ID1))*100.   | Q | 59  |
|     |    | WRITE (6,18) PCTER  | Q | 60  |
| 989 | C  | PUNCH CODE  | Q | 61  |
| 990 |    | IF (NPU) 14,14,13   | Q | 62  |
| 991 | 13 | WRITE (7,19) ID1,ID2  | Q | 63  |
|     | 14 | RETURN  | Q | 64  |
| 992 | C  |   | Q | 65  |
|     | 15 | FORMAT(1HO,T33,'TIME',T55,'FLOW 1',T76,'FLOW 2',T95,'ERROR'/T34,    | Q | 66  |
| 993 |    | 1'HRS',T57,'CFS',T78,'CFS',T97,'CFS')                               | Q | 67  |
| 994 | 16 | FORMAT (20X,F20.3,3F20.0)   | Q | 68  |
| 995 | 17 | FORMAT(1HO,T10,'ERROR STANDARD DEVIATION = ',F10.3)                 | Q | 69  |
| 996 | 18 | FORMAT(T10,'PEAK DISCHARGE ERROR = ',F7.2,' PERCENT'///)            | Q | 70  |
| 997 | 19 | FORMAT( 'ERROR ANALYSIS',T21,'ID I=',I1,T29,'ID II=',I1)            | Q | 71  |
|     |    | END   | Q | 72- |

|          |   |   |   |     |
|----------|---|---|---|-----|
| 998      |   | SUBROUTINE SEDT   | R | 1   |
|          | C | THIS SUBROUTINE COMPUTES THE SEDIMENT YIELD FOR A FLOOD             | R | 2   |
| 999      |   | COMMON CFS(300),OCFS(300,6),IEND(6),DATA(310),DA(6),DP(20),NPU,NHD  | R | 3   |
|          |   | 1,SCFS(20),C(20),A(20,6),Q(20,6),RAIN(200),DEEP(20,6),NER,MAXNO,NCO | R | 4   |
|          |   | 2MM,ICC,NCODE,DIST(6),SEGN(6),CTBLE(50,11),ITBLE(50,2),ZALFA(20),DT | R | 5   |
|          |   | 3(6),TIME,PEAK(6),ROIN,ISG(6)                                       | R | 6   |
| 1000     |   | ID=DATA(1)  | R | 7   |
| 1001     |   | SOIL=DATA(2)  | R | 8   |
| 1002     |   | CROP=DATA(3)  | R | 9   |
| 1003     |   | CP=DATA(4)  | R | 10  |
| 1004     |   | SL=DATA(5)  | R | 11  |
|          | C | COMPUTE SEDIMENT YIELD  | R | 12  |
| 1005     |   | X=ROIN*DA(ID)*53.333*PEAK(ID)                                       | R | 13  |
| 1006     |   | SED=95.*X**.56*SOIL*CROP*CP*SL                                      | R | 14  |
| 1007     |   | WRITE (6,3) SED   | R | 15  |
|          | C | PUNCH CODE  | R | 16  |
| 1008     |   | IF (NPU) 2,2,1  | R | 17  |
| 1009     | 1 | WRITE (7,4) ID,SOIL,CROP,CP,SL                                      | R | 18  |
| 1010     | 2 | RETURN  | R | 19  |
|          | C |   | R | 20  |
| 1011     | 3 | FORMAT (10X, 'SEDIMENT YIELD = ', F10.1, ' TONS')                   | R | 21  |
| 1012     | 4 | FORMAT( 'SEDIMENT YIELD',T21,'ID=',I1,T29,'SOIL=',F5.3,T42,'CROP    | R | 22  |
|          |   | 1=',F5.3,T57,'CP=',F5.3,T70,'LS=',F5.3)                             | R | 23  |
| 1013     |   | END   | R | 24- |
| //\$DATA |   |   |   |     |



ZALFA = 1234567890 \*.,-

COMMAND TABLE

|                      |       |
|----------------------|-------|
| START                | 1 2   |
| STORE HYD            | 2310  |
| RECALL HYD           | 3310  |
| COMPUTE HYD          | 4310  |
| PRINT HYD            | 5 2   |
| PUNCH HYD            | 6 1   |
| PLOT HYD             | 7 2   |
| ADD HYD              | 8 4   |
| STORE RATING CURVE   | 9100  |
| COMPUTE RATING CURVE | 10310 |
| STORE TRAVEL TIME    | 11100 |
| COMPUTE TRAVEL TIME  | 12 5  |
| ROUTE                | 13 4  |
| ROUTE RESERVOIR      | 14100 |
| ERROR ANALYSIS       | 15 2  |
| SEDIMENT YIELD       | 16 5  |
| FINISH               | 17 0  |

